Joint Sealing and Re-Sealing

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Why Do We Make and Seal Joints (Owner)

To Control Cracking

Controlled Cracking



Uncontrolled Cracking



Types of Saw Cuts

Initial Saw Cut



Reservoir Cut



Is Sealant Cost Effective?

FHWA Sealant Effectiveness Study



Performance of Sealed and Unsealed Concrete Pavement Joint:

This TechBrief presents the results of a nationwide study of the effects of transvers joint sealing on performance of jointed plain concrete pavement (JPCP). This stud, was conducted to assess whether JPCP designs with unsealed transverse joints performed differently from JPCP designs with sealed transverse joints. Distress and deflection data were collected from 117 test sections at 26 experimental joint seal ing projects located in 11 states. Performance of the pavement test sections with unsealed joints was compared with the performance of pavement test sections wo one or more types of sealed joints.

BACKGROUN

The sealing anansverse. traction joints in JPCP has been standard pt ted States for many years. Its widespread tice throu out much of the is due to common belief t sealing joints improves concrete pavem in two ways: by lucing water infiltration into the pavem rforma eby reducing th ture, courrence of moisture-related distresses su æ , wing Sulting by preventing the infiltration of incompre stones) into the joints, thereby reducing the lik ibles a sand a sure-related joint distresses such as joint spalling and blowur nod of h oints in jointed concrete pavement (JCP) are typically crea by making a mitial saw cut to force controlled cracking, followed by a s ond, wider saw cut to produce a reservoir for the joint sealant material. T ditional approach of sawing and sealing transverse contraction joint anated to account for between 2 and 7 percent of the initial construct cost of a JCP. Moreover, these sealed transverse joints require resealing (or more times over the service life of the pavement, leading to additio costs in terms of labor, materials, operations, and lane closures.

Recently, several State departments of transportation (DOTs) have be questioning conventional transverse joint sawing and sealing practices. Th agencies contend that the benefits derived from sealing do not offset the α associated with the placement and continued upkeep of the sealant over life of the pavement. As a result, they have been experimenting with diff... ent sawing and sealing alternatives, for example:

- Narrow unsealed joints, consisting of single saw cuts that are left unsealed.
- Narrow filled joints, consisting of single saw cuts that are filled with sealant that adheres to the sides and bottom of the saw cut.
- Narrow sealed joints, consisting of single saw cuts that contain a narrow backer rod and sealant material.

AASHTO New Design Guide



US.Department of Transportation Federal Highway Administration

TechBrief

The Concrete Pavement Technol-

onal effort to improve

ogy Program (CPTP) is an inte-

the long-term performance and

cost-effectiv eness of concrete

pavements. Managed by the Federal Highway Administration through partnerships with State

highway agencies, industry, and

academia, CPTP's primary goals

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to produce user-thlendly software

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and rehabilitation of concrete

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Reasons for Joint Sealing



Why Seal Joints and Cracks

Prevents Incompressible from Lodging in the Joint — Slab Growth and Blow Ups

Why Seal Joints and Cracks

PCCP

SOIL

SUBGRADE "ABC"

Prevents Water from Entering the Subgrade:

-Prevents subgrade erosion -Voids beneath



How Do You Design the Joint Sealant System (Owner)

Reservoir Design and Cutting





Good for Hot Pour Bad For Silicone OK For Hot Pour

Good for Silicone

Bad For Silicone



Ton, E., "Factors in Joint Seal Design, "Highway Research Record No. 80, Highway Research Board, National Research Council, 1965

Sealant Types

Silicone Non Sag Self Leveling Rapid Cure







Hot Pour Standard Modulus Low Modulus

Compression Seal









Allowable Joint Opening Movements (Compression/Extension)

- Hot Pour Sealants: 25% Extension
- Silicone Sealants: 50% Compression to 100% Extension
- Compression Seals: 15% min
 Compression to 50% Extension

Manufacturer Design Tables Silicone and Compression Seal

*Joint Width	1/4"	3/8"	1/2"	5/8"	3/4"	7.	/8"	1"	1 1/8"	1 1/4"	1 3/8	i" 1 1/2"
Minimum Sealant	1/4"	1/4"	5/16"	5/16"	3/8"	3	/8"	3/8"	1/2"	1/2"	1/2'	' 1/2"
Recess					Meeting Sp	ecification	s					A CONTRACTOR OF
Backer Rod Diameter ¹	3/8"	1/2"	5/8"	3/4"	Delastic [®] Preformed Pavement Seals meet ASTM standard specifications. They are also recognized by the FHWA, U.S. Army Corps of Engineers, the U.S. Air Force, the FAA, consulting engineers and other agencies as an effective, long-lasting concrete pavement joint seal solution.							
Sealant Bead Thickness	1/4"	1/4"	1/4"	5/16'	Delastic [®] Preformed Pavement Seals have been successfully used on high per- formance concrete pavements throughout the U.S. Many of these installations have protected pavements located in extreme hot and cold climates in excess of 20 years.							
												ary bases all over the world rely Pavement Seals.
Minimum Joint Saw/Reservoir Depth	1 1/8"	1 1/4"	1 1/2"	1 3/4								
Minimum Backer Rod Depth	1/2"	1/2"	5/8"	11/16	6 Typical joint design for the "E" and "V" series pavement seals Delastic [®] Preformed Pavement Seal Characteristics							Compression Seal at DFW
					Delastic [®] Seal Characteristics			- I	oint Design Criteria			
					Seal Catalog No.	Nominal	Nominal	Max.	Narrowest	Widest	Minimum	Typical Installed Width (A)**
Estimated Llagge Non	245	140	440	70	E-437	0.437 (11.11)	0.937 (23.81)	0.153 (3.88)	0.219 (5.56)	0.372 (9.45)	1.000 (25.40)	0.250 (6.35)
Estimated Usage Non-	245	149	112	70	E-562	0.562 (14.29)	0.625 (15.88)	0.188 (4.78)	0.290 (7.37)	0.478 (12.14)	1.063 (27.00)	0.3125 (7.94)
Sag					E-686	0.687 (17.46)	0.687 (17.46)	0.259 (6.59)	0.325 (8.26)	0.584 (14.84)	1.188 (30.18)	0.375 (9.53)
_					E-816	0.812 (20.64)	0.830 (21.08)	0.313 (7.95)	0.378 (9.59)	0.691 (17.54)	1.438 (36.53)	0.500 (12.70)
Estimated Usage					E-1006	1.000 (25.40)	1.000 (25.40)	0.450 (11.43)	0.400 (10.16)	0.850 (21.59)	1.625 (41.28)	0.500-0.5625 (12.70-14.29)
					E-1256	1.250 (31.75)	1.000 (25.40)	0.563 (14.30	0.500 (12.69)	1.063 (26.99)	1.875 (47.63) 2.250 (57.15)	0.750 (19.05)
Self-leveling(ft./gal)	273	172	130	82	E-2000	2.000 (50.80)	1.500 (38 10)	0.950 (24 13	0.750 (19.05)	1.700 (43.18)	2.500 (63.50)	1.125 (28.58)
					E-2500	2.500 (63.50)	2.500 (63.50)	1.125 (28.58	1.000 (25.40)	2.125 (53.98)	3.375 (85.73)	1.375 (34.93)
					E-3000	3.000 (76.20)	2.500 (63.50)	1.550 (39.37) 1.000 (25.40)	2.550 (64.77)	4.000 (101.60)	1.750 (44.45)

Above: First number shown in bold represents inches, metric dimensions (mm) are shown in parentheses. Notes:*Thickness of the seal wall and internal web are not drawn to scale. 1 Maximum movement which seal will accommodate in joint with correct design. 2 A narrower opening will place excessive stress on the seal and may cause premature failure. 3 A wider opening may not provide sufficient compressive force to hold the seal in place.** To be used as reference only. Installed width may vary by project.

Silicone Joint Sealant Configuration

Non-Sag

Self-Leveling





Recess min 1/4"- 3/8" Below Surface
 2 to 1 Ratio
 Tooling Required

Hot Pour Joint Sealant Configuration

40° F Minimum Pavement Temperatures Flush Fill, Recessed or <u>Over-band</u> _ _ 3

Flush Filled



Recessed

Flush Filled



Shipping And Storing Materials (Contractor)

Asphalt Hot Pour Joint/crack Sealants

•ASTM D-6690:

Type I - ASTM D1190

Type II - ASTM D3405

Type III – Low Modulus

Type IV - Fed Spec SS-S-1401C

FAA P 605-ASTM D-6690

State Specifications



SILICONE PACKAGING

- Drums-50 gals of Material
- **5** Gallon Pails
- 29 oz. Tubes (6 per case)
- Store out of direct sun

Do not store in freezing temperatures or above 90°F. Keep out of excessive humidity



How Are Materials Tested?

- Certification
- Owner Laboratory
- Outsourced Testing



Joint Sealant Installation (Contractor)



Power Washing After Green Sawing







Personal Protective Equipment





Inserting and Rolling Backer Rod

BACKER ROD 25% Larger than Joint Cold Rod/Hot Rod Closed Cell Backer Rod Do Not Puncture Backer Rod-buobling Do Not Stretch Backer Rod

Installing Sealant



Compression Seal Installation



- Lubricant-Adhesive shall meet ASTM D2835
- Installation Above 32 F
- Install Sealant in Longitudinal Joint First
- Cut Longitudinal Joint in Center of Each Transverse Joint
- Install Transverse Joint Continuously Across
- Sealant Stretch Should be Less than 4 %
- Recess Sealant 3/16"



Sealant Acceptance (Owner)

Defining Sealant Life

TPP Pavement Maintenance			Time at Which 75% Effectiveness Level Was Reached, months *					
	Sealant	Config-					South	
Materials: SHRP Joint Reseal	Material Keeb 0005	uration	Arizona	Colorado	Iowa	Kentucky	Carolina	Average
	Koch 9005	2	110	66	94	101	0.0	99
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UBLICATION NO. PHWA/hD/89-142 SEPTEMBER 1	RS 231	2	135	69	118	108	138	114
		3			103	155	80	113
		4	83	72				78
	Meadows	1		34	40	39	55	42
	Sof-Seal	2	Sector Sector	40	51	64	46	50
		3	a har backet	a station of the	57	161	31	83
		4	Strength Strength and strength	43		COLUMN TO A COLUMN		43
\sim Cratco 221 = 5.4 – 9.8 vrs	Koch 9030	1		31	50	60	41	46
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232% to 348% increase for	Dow 888-SL	1	183	110	125	164	186	154
Cilicone	Mobay 960-SL	1	194	93	65	115	168	127
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dou Georgetown Frite IcLean, VA. 22101-2296	Koch 9005	1		and the second second	and and a	173	See Strates	173

Times greater than 82 months are extrapolated to a maximum of 200 months.

Arizona SPS-2 Silicone Sealant Life



Arizona Sealant Performance

SPS-2 I-10

Technical Memorandum Arizona SPS-2 PCC Joint Seal Performance

Overview

The Arizona Special Pavement Studies (SPS) 2 jointed concrete pavement test site, located on eastbound I-10 between mileposts 106 and 109 was constructed in 1993 with 12 LTPP and 9 ADOT test sections. Each test section includes about 33 transverse joints, spaced at 15 ft, which were reportedly sealed using Crafco 34902 non-sag RoadSaver Silicone sealant. Various combinations of base type, concrete strength, slab width, and slab thickness, as shown below, were designed to allow statistical analysis of the contributions of each factor. A March 2013 evaluation of the condition of the joints and seals indicates correlations of base type and Portland cement concrete (PCC) strength with adhesion and sliver spall failures.

		PCC				
		Strength,	Slab	Thickness,		
Section	Base*	psi	width, ft	in		
213	DGAB	550	14	8		
214	DGAB	900	12	8		
215	DGAB	900	12	11		
216	DGAB	900	14	11		
217	LCB	550	14	8		
218	LCB	900	12	8		
219	LCB	550	12	11		
220	LCB	900	14	11		
221	PB/DG	550	14	8		
222	PB/DG	900	12	8		
223	PB/DG	550	12	11		
224	PB/DG	900	14	11		
262	DGAB	550	14	8		
263	PB/DG	550	14	11		
264	PB/DG	550	12	11		

^{*} 6-in dense graded aggregate (DGAB); 4-in PBTB/4-in DGAB (PB/DG); 6-in Lean Concrete (LCB)

Transverse Seal Findings

Overall performance of the SPS-2 joint seal systems is extraordinarily good, considering the seals have been in place for 20 years and the truck lane has carried about 31 million Equivalent Single Axle Loads (ESALS). As figure 1 illustrates, no section exhibits more than 35 percent overall seal failure with six sections remaining below ten percent. Five randomly-selected transverse joints were evaluated in each section.



Figure 1. Overall failure rates on transverse joints

Primary modes of failure include sliver spalls and loss of adhesion with the joint walls. Additionally, slight cohesive failure was identified when the installed seal thickness (less than 0.125 in) fell below the design thickness (0.25 in). Full depth sliver spalls, shown in figure 2, typically progress around or through the aggregate adjacent to the joint wall.

These sliver spalls accounted for more than 65 percent of the seal system failures with 2.4 times more failure noted in 550 psi than the 900 psi compressive strength SPS-4 US 60

evaluated. Other sealant types, such as the hot-applied seals, that had reached more than \$5 percent failure in 2002, were not included in this evaluation). Silicone seal failure modes included full-depth adhesion loss, full-depth sliver spalls (typically less than 1 in long and 0.5 in wide), and occasional full-depth cohesion loss. Several of these failure modes are shown in figure 3. Figure 4 provides a summary of the failure types and amounts noted for each combination of sealant and joint configuration.





Figure 3. Failure modes of joint seal materials at the Mesa SPS-4 site. Figure 4. Seal failure levels by type after 15 years.

Statistical Analysis

Using the data collected and assembled, an analysis of variance (ANOVA) was conducted to determine joint seal effectiveness and the effect of sealing on pavement performance by answering the following questions:

- Is there a statistically significant difference in the overall 2006 seal performance? Also, rank the seal/joint configurations combinations evaluated according to their 2006 performance.
- Is there statistically significantly more spalling in the wheelpaths?
- Is spalling statistically greater for the combinations of seal/joint configurations evaluated?
- Is measured faulting significantly influenced by the presence of seals (i.e., no seal, partial, or well sealed joints)?
- Is there a statistically significant difference in faulting when measured 1- or 2.5-ft from the slab edge?

Summary of Results, Conclusions, and Recommendations

Results of the statistical analysis are presented in table 2. Based on the results shown, the following conclusions and recommendations are given for ADOT joint seal design:

- Overall, silicone sealants (placed using configuration C) had the least amount of adhesion failure, cohesion failure, and sliver spalls. Neoprene sealants (placed using configuration C) had the most distress. Silicone sealants (placed using configurations A & B) experienced moderate levels of distress.
- Statistically significantly more spalling was observed in the wheelpath areas across a
 joint as compared to the non-wheelpath areas. This observation was true for both sealed
 (i.e., all joint configurations and sealant types evaluated) and unsealed joints. The level of
 spalling was, however, low and thus not significant from an engineering point of view.
- In general, joints fully sealed with silicone reported significantly higher levels of spalling (all joint configurations) than the other seal/joint configuration types. The joints with the

When to Reseal & Sealant Longevity

Adhesive Failures Cohesive Failures % Damaged or Missing

When the Sealant is No Longer Serving its Intended Function







- Design Joint Sealant System for the Expected Joint Movements
- Select a Joint Sealant Material and Backer Rod Appropriate for the Intended Purpose
- Ensure Proper Cleaning and Preparation– Clean, Dry and Bondable
- Inspect the Work and Verify its
 Acceptability
NHI Training: Constructing Quality PCC Pavement Preservation Treatments

- How to Construct Durable Full-Depth Repairs in Concrete Pavements (FHWA-NHI-134207A)
- How to Construct Durable Partial-Depth Repairs in Concrete Pavements (FHWA-NHI-134207B)
- Proper Diamond Grinding Techniques for Pavement Preservation (FHWA-NHI-134207C)
- Proper Construction Techniques for Dowel Bar Retrofit (DBR) and Cross-Stitching (FHWA-NHI-134207D)
- Proper Joint Sealing Techniques for Pavement Preservation (FHWA-NHI-134207E)





Adding Longevity to Concrete Roads





Concrete Pavement Preservation



Why Concrete Pavement Preservation Bellefontaine, Ohio 1925



Court Avenue is 130 Years Old



Concrete Pavement Preservation Guide

CONCRETE PAVEMENT PRESERVATION GUIDE



IOWA STATE UNIVERSITY

National Concrete Pavement Technology Center

AUGUST 2022



Grinding Versus Milling



Standard Milling Head

Grinding Head





Damage from Milling ARFC of PCCP

Before

1 inch

Milling Vs Grinding

Diamond Grinding

Joint Damage from Milling Machine

Original Texture

Diamond Blade Components



Spacers Are Used To Separate the Cutting Blades



How Blades Create the Corduroy Texture



Why Blade Spacing is Important



60 Blades vs 52 Blades per Foot



Well Constructed Texture



Diamond Grinding Equipment



Frames on Diamond Grinder





Grinding Close to Barriers and Obstructions









Diamond Grinding Slurry



Slurry Recovery Failure



Proper Slurry Recovery System



Poor Recovery

IGGA Best Management Practices for Slurry Handling





The iterational Growing II: Givening-Association (1024) is a new prefit hande Association funded in 727 by a page of dedicated indiaxity prohesional amenited to be velocingened of the dament giveding parks (process for suchas constraints) with Perturbation means methods and aptical in 1026, the IEEA joined in alfitation with the American Concess Deserved Association (ACMV) to represent to newly formed Concerns Permission Biotracian Division. The IEEA J ACM CPU (Neikon new arems as the to fract rescurs and instally properticially in the material optical priority and provide and the second provide and and aptical in the second and instally methods. The material priority aptication provide provide and provide and provide and provide and approximation and proper use of classical formed participations) and the CEGA to serve as the lander promotional and borthold resources to astrophone: and proper use of classical provide part oppositions) and the CEGA to serve as the lander promotional and borthold resources to astrophone: and proper use of classical provides part oppositions) and an ACC promotion promotion providence of the CEGA to be provide and provide the total to be astrophone and proper use of classical provides part oppositions) and the ACC provides to the total provides of the total provides and provides to the total provides of the total total total provides to the total provides and the total total provides and provides to the total provides and the total total provides to the total total total total total total total total provides total total provides total t

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NGYL

Poor Match Between Passes





Holidays





Different Types of Full Depth Repair



Full-Depth Repair Use

Purpose

- Restore Structure
- Restore Ride
- Used For
 - Joint Deterioration
 - Transverse Cracking
 - Longitudinal Cracking
 - Broken Slabs and Corner Breaks

Repairing Cracking



Longitudinal Cracks

Corner Breaks

Repairing Broken Slabs



Repairing Joint/Crack Deterioration



Types of Distress That Cannot Be Addressed





Excessive Pavement Deterioration

What Is A Full Depth Repair



Full Depth Repair Process

- Identify and Mark Areas
- Selection of Materials
- Sawing Repair Boundaries
- Removal Methods
- Base Preparation
- Installing Dowels and Tie Bars
- Casting and Finishing Slabs

Identify and Mark Repair Areas



6 Ft Minimum Width Requirement



Repair Boundary Determination



- A. Minimum patch length is 6 feet for doweled joints; 8 to 10 feet for aggregate interlock joints.
- B. Check distance between patches and nearby joints.
- C. Replace the entire slab if there are multiple intersecting cracks.
- D. Extend the patch beyond joint by about 1 foot to remove existing dowels, even if there is not any deterioration to that side of the joint.
- E. When marking partial-width patches for longitudinal cracks, keep the joint off of the wheel paths.

Materials

Materials Used in Full-Depth Repair

- Patching concrete
 - Ready-mixed concrete
 - Field-mixed concrete
 - Proprietary fast-setting mixtures
- Dowels
- Dowel bar epoxy or grout
- Plastic grout retention disks
- Curing compound
- Joint sealant




How Patching Materials Are Selected

- To meet specification provisions:
 - 28-day strength
 - Freeze-thaw resistance
 - Durability
 - Opening to traffic (early strength)
 - Matching color
- Can incorporate:
 - Conventional cements
 - Accelerating admixtures
 - Specialty or proprietary cements
 - Proprietary factory-blended mixtures







Sawing Repair Boundaries





Pressure Relief

Perimeter Cut

Two Types of Longitudinal Joint Face

- Smooth-faced, separated longitudinal joint
 - For repairs less than one slab length (usually 15 feet or less)
- Smooth-faced, tied joint
 - For repairs greater than one slab length (usually more than 15 feet)
- Both require same perimeter sawing





Sawing Procedure for Full-Depth, Transverse Cuts

- Set cut depth to fully reach slab bottom
 - Nominal thickness plus 1/2 inch
- Saw toward any live traffic lane and avoid turning your back on traffic if possible (use spotter if necessary)
- If saw blade binds then use pressure-relief cut in patch area
- Determine if over-sawing is acceptable
 - OK if sawing over existing joint
 - OK if sawing into shoulder
 - Avoid if would weaken an adjacent traffic lane

The rule of thumb is to set the depth to the nominal thickness plus 1/2 inch.





Removal Methods



Pin and Chain

Drill holes

- One-piece requires 20-degree angled holes (opposing)
- Two-piece uses compression fit in vertical holes
- Insert pins
- Secure chains to loader bucket or excavator and lift out



Drilling 20° Angled Holes for Lift Pins



One-piece

Pin

Two-piece

Pin

Torque Claw

- Mount claw to equipment
- Make relief cut
- Angle into position
- Lift out





Lateral Pressure

- Mount attachment to equipment
- Drill holes
- Insert device pins on equipment
- Apply pressure
- Lift out



Vacuum Suction

- Mount attachment to equipment
- Position vacuum pad over repair area
- Apply suction
- Lift out



Base Preparation

- Check the base for the following:
 - Disturbed (need leveling)?
 - Soft or saturated?
 - Standing water evident?
- Drain any standing rainwater
- Dry excessive moisture



Restore, Grade, and Compact

- Add new base material, if needed
 - Backfill utility excavation
 - Replace soft materials
- Compact base
 - Use vibratory plate compactor with 4,000–6,000-lb. centrifugal force rating
 - Consider roller for larger patch areas



Checking Perimeter Edges

- Look for:
 - Damage to perimeter joint from removal operations
 - Distress that was not fully removed
 - An inadequate joint face for anchoring dowels or tiebars (sounding)
- If damage is evident:
 - Cut back perimeter
 - Remove concrete
 - Compact base along new edge



Dowels and Tiebars

- Dowels
 - Smooth, round
 - Intended to allow slippage
 - Diameter (1.25 to 1.5 inches)
 - Specifications:
 - AASHTO M254 Standard Specification for Corrosion-Resistant Coated Dowel Bars
 - ASTM A1078 Standard Specification for Epoxy-Coated Steel Dowels for Concrete Pavement
 - Purpose: load transfer

NOTE A: Tie bars are used only if the pavement joint was designed to be tied and then only if repair is full slab length or at least 15 feet long;



- Rebar or tie bars
 - Deformed
 - Intended to hold in concrete
 - For full-depth repair, diameter usually:
 - #4 (1/2 inch)
 - o #5 (5/8 inch)
 - #6 (3/4 inch)
 - Typical length is 36 inches
 - Specifications: AASHTO M31; ASTM A615; ASTM A934
 - Purpose: hold joint or crack closed

Handheld Drilling

- Mobile
- Needed in cases of tight access
- Slower drill speed
- Adequate for small projects or low number of holes
- Less alignment control
- Adequate for tie bars



Reference for Drilling

Slab Referenced

Base Referenced



Slab Referenced Drill

- Ganged (up to 5)
- Self-propelled or mounted to other equipment
- Wheels ride on slab to position drill bit
- Simultaneous drilling controls



Boom Mounted Drills

- Ganged (up to 6)
- Mounted to backhoe or other equipment
- Rotates 360 degrees to drill both sides of repair
- Simultaneous drilling controls



Anchoring Dowel Bars or Tie Bars

Step 1: Clean the Hole

Step 2: Mix and Place Bar Anchoring Material

Step 3: Insert Dowels and Tie Bars

Step 4: Place Grout Retention Disk and Oil Bar

Mixing and Insertion Procedure



Place Grout Retention Disk & Oil Bars

- Place disk over bar before inserting dowel
- Ensure some material is evident through weep hole after bar is inserted
- Alternatively, trowel extra grout around bar at joint face
- Lightly oil protruding end of dowel





Preparing Longitudinal Joint and Installing Separator

- Use minimum 1/4-inch thick separator for repairs less than one slab length (typically 15 feet)
- Place only along longitudinal edges with existing concrete lane or shoulder
- Typical materials:
 - Asphalt fiberboard
 - Closed-cell polypropylene foam
- Cut to match depth and length of edge



Concrete Placement



- Place from chute to distribute
- Keep drop height below 3 feet
- Avoid excessive shoveling
- Consolidate with spud vibrator
 - Stay vertical
 - Do not drag through concrete
 - Avoid touching dowels or rebar

Finish and Texture, Finish the Surface





- Only use well-maintained equipment
 - Screed should be straight, true
 - If mechanical, moving parts greased
- Coordinate timing closely with placement
 - Fast-setting mixes less working time
 - Don't add water to help finishing
- Overlap edge at least 6 to 12 inches with screed
- Repeat 2 to 3 times if hand screeding



Using Skid Steer Screed



Texturing Repair Surface

- Match texture of concrete as close as possible
- Practical options (broom, tine)
- Consider:
 - Direction of texture
 - Distance between combs (for tining)
- Texture as soon as possible after finishing
 - Apply with consistent pressure on tool



Applying Curing Compound

- Apply soon after final finishing
 - Use power-driven sprayer for even nozzle pressure
 - Apply evenly to the surface at rate of 1 gallon per 200 sq. ft.
 - Clean nozzle periodically
- Cover the repair surface completely
 - Properly applied curing compound should resemble a solid sheet of white

paper





GOOD

POOR









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Means for Improving pH prior to Slurry Recovery and Disposal



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