

Asphalt Binder Characteristics Affecting Durability Cracking

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11th Arizona Pavements/Materials Conference

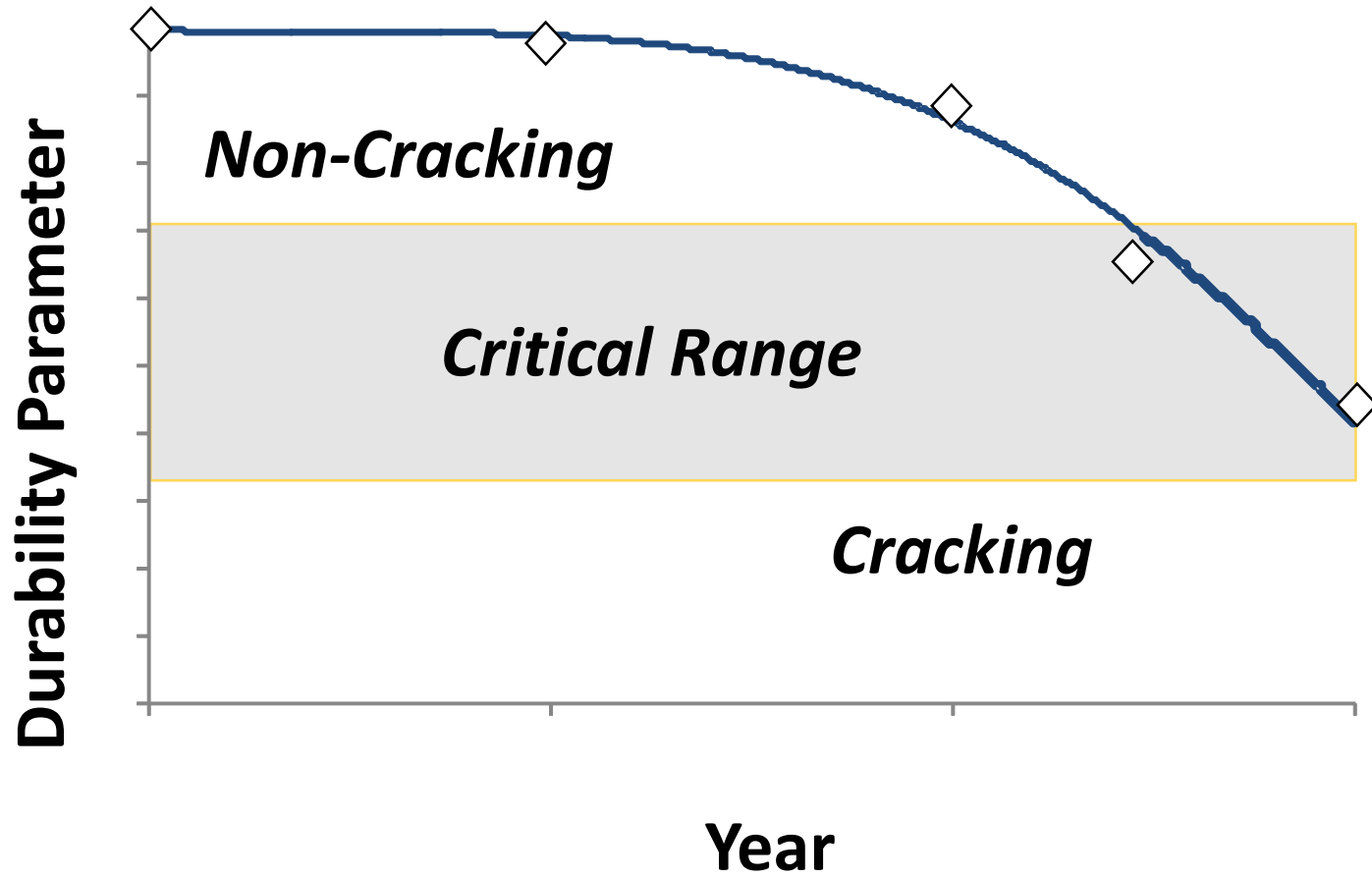
November 19-20, 2014

Tempe, AZ



- TPF-5(153) Optimal Timing of Preventive Maintenance for Addressing Environmental Aging in Hot-mix Asphalt Pavements
 - MN, MD, OH, TX, WI, LRRB
 - Thomas J. Wood, Lead Agency Contact
- Airfield Asphalt Pavement Technology Program (AAPTP) Project 06-01
 - Techniques for Prevention and Remediation of Non-Load-Related Distresses on HMA Airport Pavements
 - AAPTP sponsors and research panel
- Member Companies of the Asphalt Institute

- Asphalt Institute
- AMEC
 - Doug Hanson, Researcher
- Consultant
 - Gayle King, Researcher



- In-service aging leads to oxidation and loss of flexibility at intermediate and low temperatures
 - Block-cracking
 - when environmental (non-load) conditions create thermal stresses that cause strain in the asphalt mixture that exceeds the failure strain

- In-service aging leads to oxidation and loss of flexibility at intermediate and low temperatures
 - Preventing or mitigating distress
 - identify a property of the asphalt binder or mixture that sufficiently correlates with its flexibility
 - provide a procedure to monitor when flexibility reaches a state where corrective action is needed

- A durable asphalt:
 - has physical properties necessary for desired initial product performance, and
 - is resistant to change in physical properties during long-term, in-use environmental aging

Petersen, J.C., “Chemical Composition of Asphalt as Related to Asphalt Durability-State of-the-Art”, TRR. 999, 1984

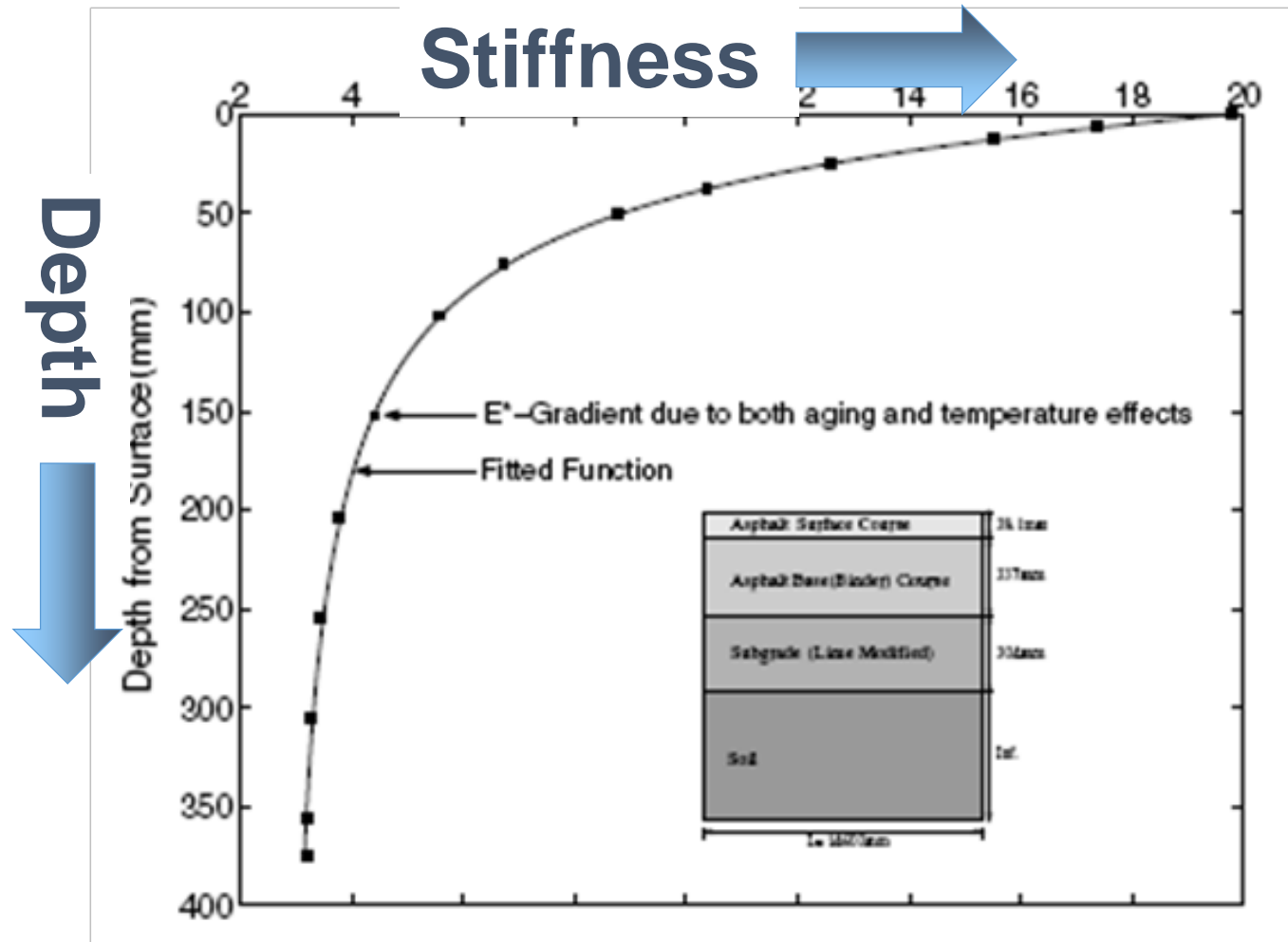
Vallerga: Age-Embrittlement



Raveling

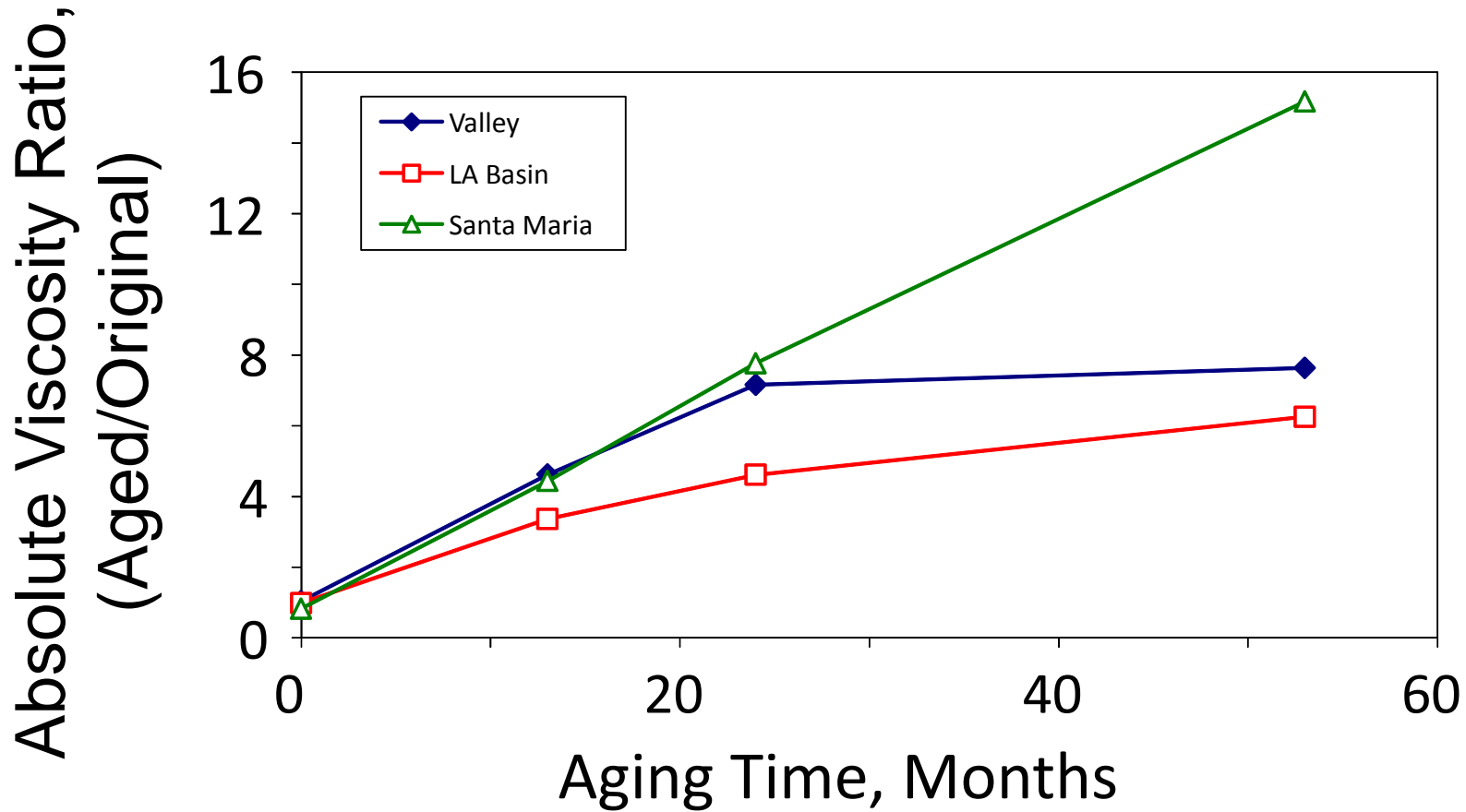


Block Cracking



- Physical Changes – Ductility
 - Block cracking severity related to ductility at 60°F (15°C) – Kandhal (1977)
 - “Low-Temperature Ductility in Relation to Pavement Performance”, ASTM STP 628, 1977
 - Loss of surface fines as ductility = 10 cm
 - Surface cracking when ductility = 5 cm
 - Serious surface cracking when ductility < 3 cm

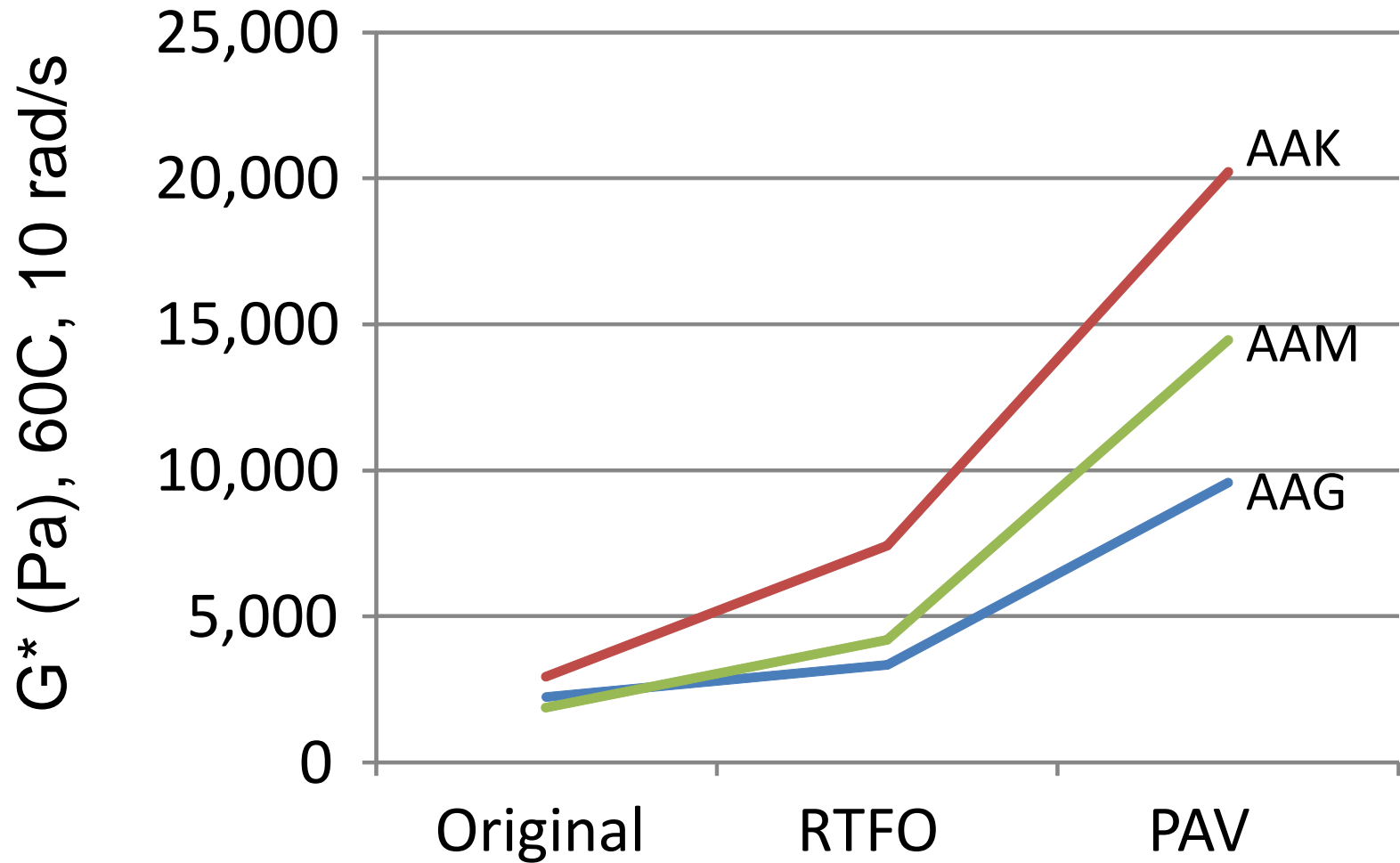
1981 CA Durability Study



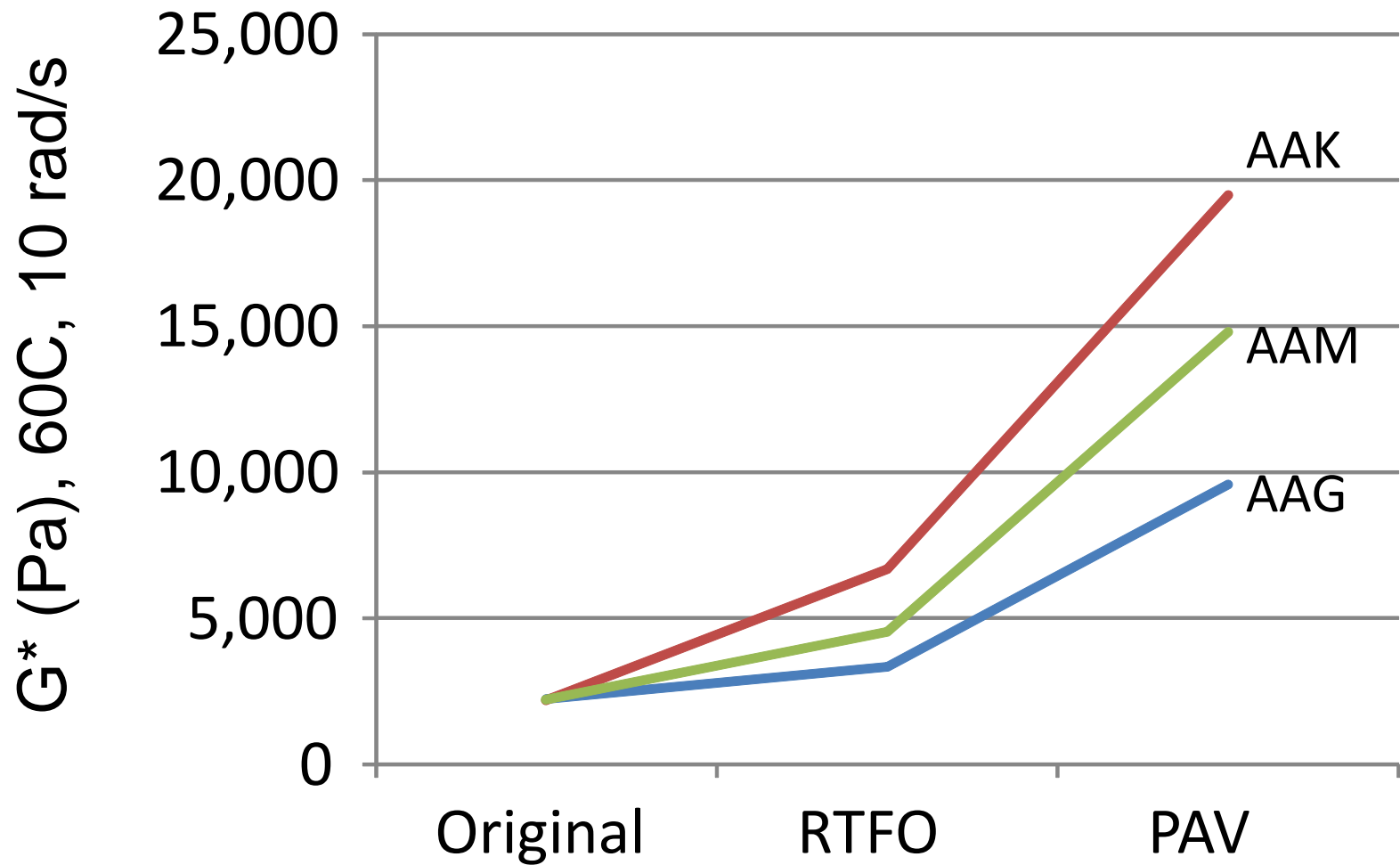
Kemp, et.al.

Sacramento (62.9C), 7-9% Air Voids, Non-Absorptive Aggregate

Rate of Aging



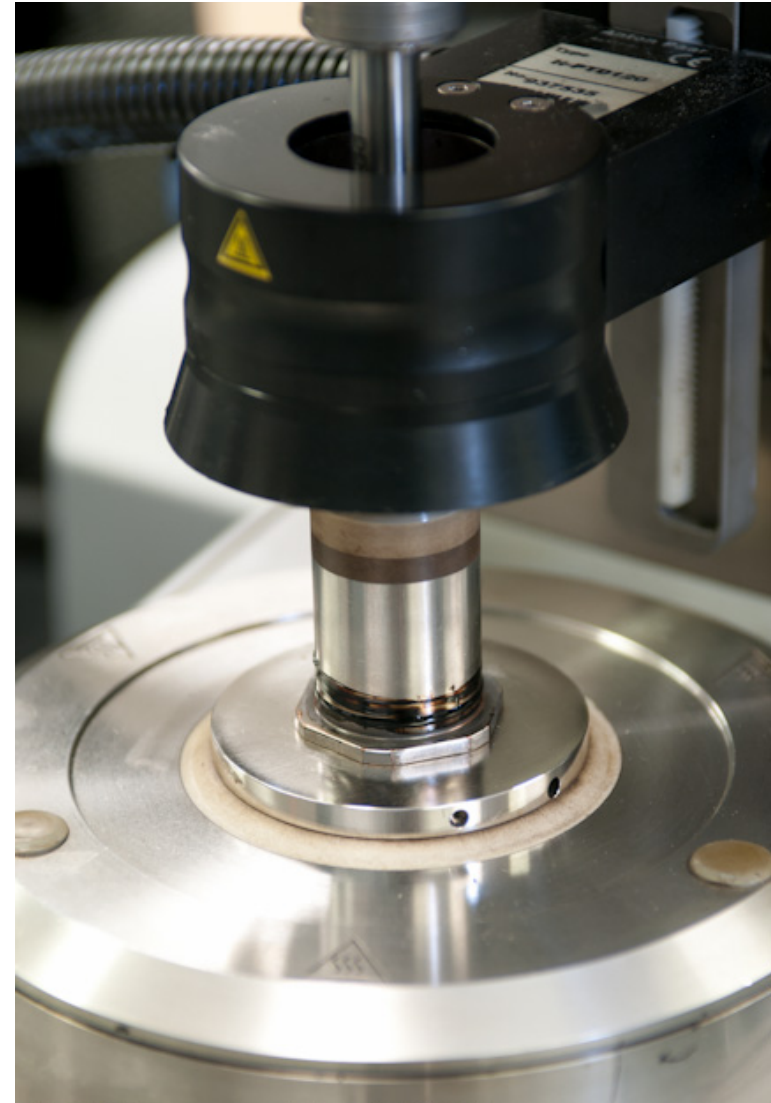
Rate of Aging (Normalized – Original)



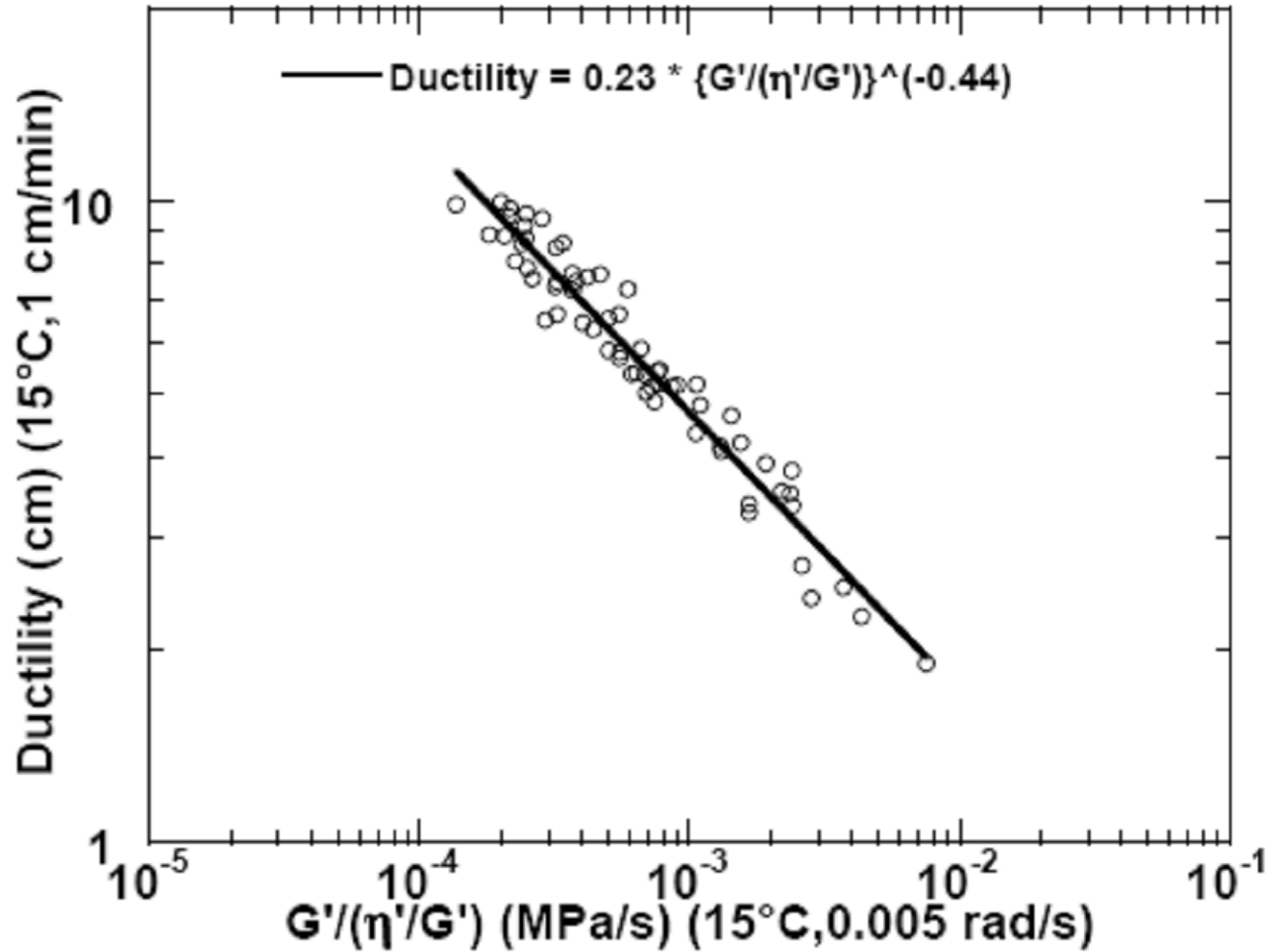
- Texas A&M Research (Glover, et.al.)
 - 2005
 - “Development of a New Method for Assessing Asphalt Binder Durability with Field Evaluation”
 - Build on work by Kandhal suggesting block cracking and raveling is related to low binder ductility after aging
 - Identified rheological parameter related to ductility

Dynamic Shear Rheometer

- Mastercurve at 15°C
 - 8-mm parallel plate
 - 5, 15, and 25°C
 - Frequency sweep (0.1 to 100 rad/s)
 - Obtain Texas A&M parameter at 0.005 rad/s
 - $G' / (\eta' / G')$
 - Related to ductility at 15°C and 1 cm/min.



Ductility and DSR Parameter

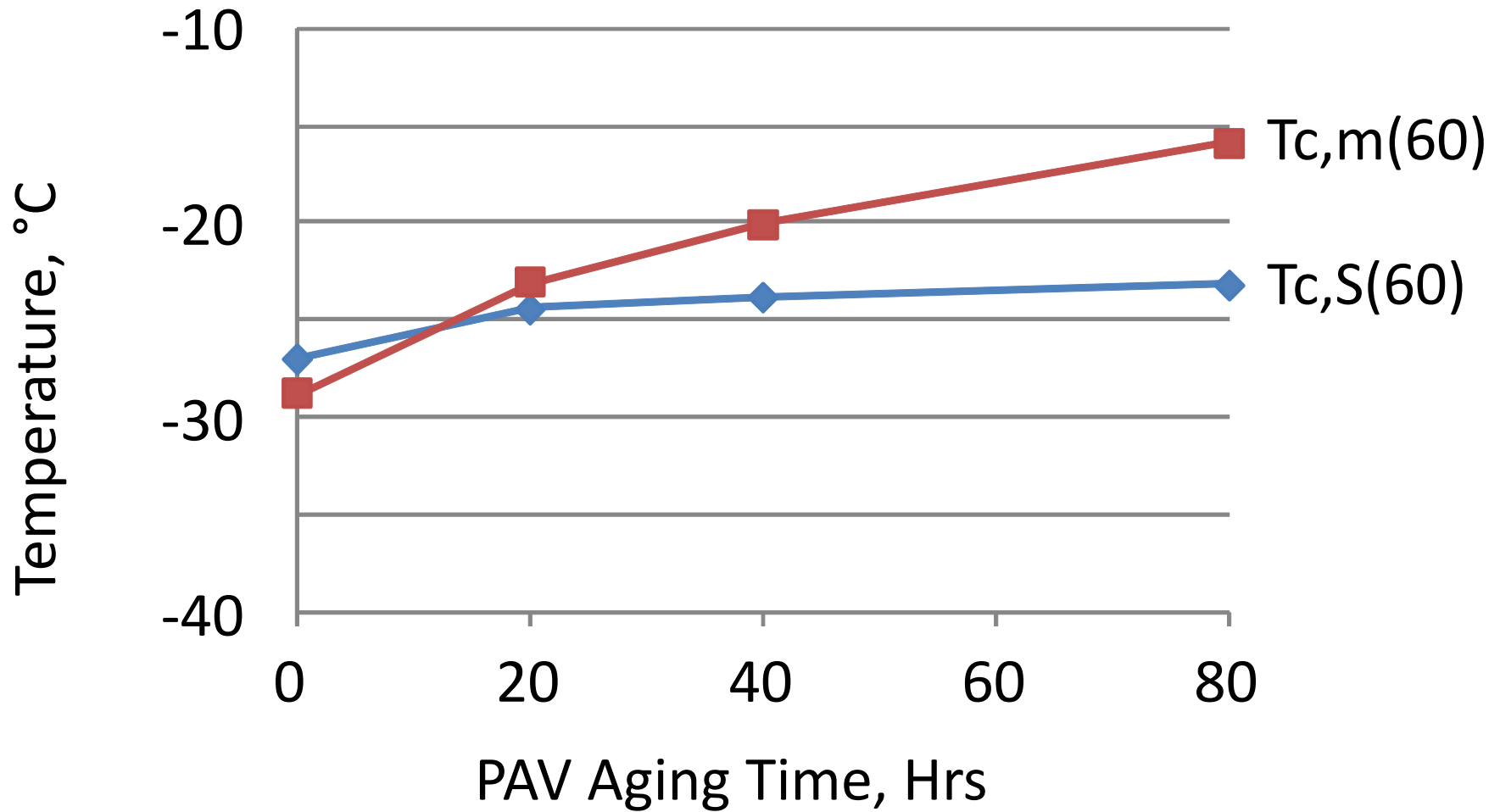


(Glover et.al., 2005)

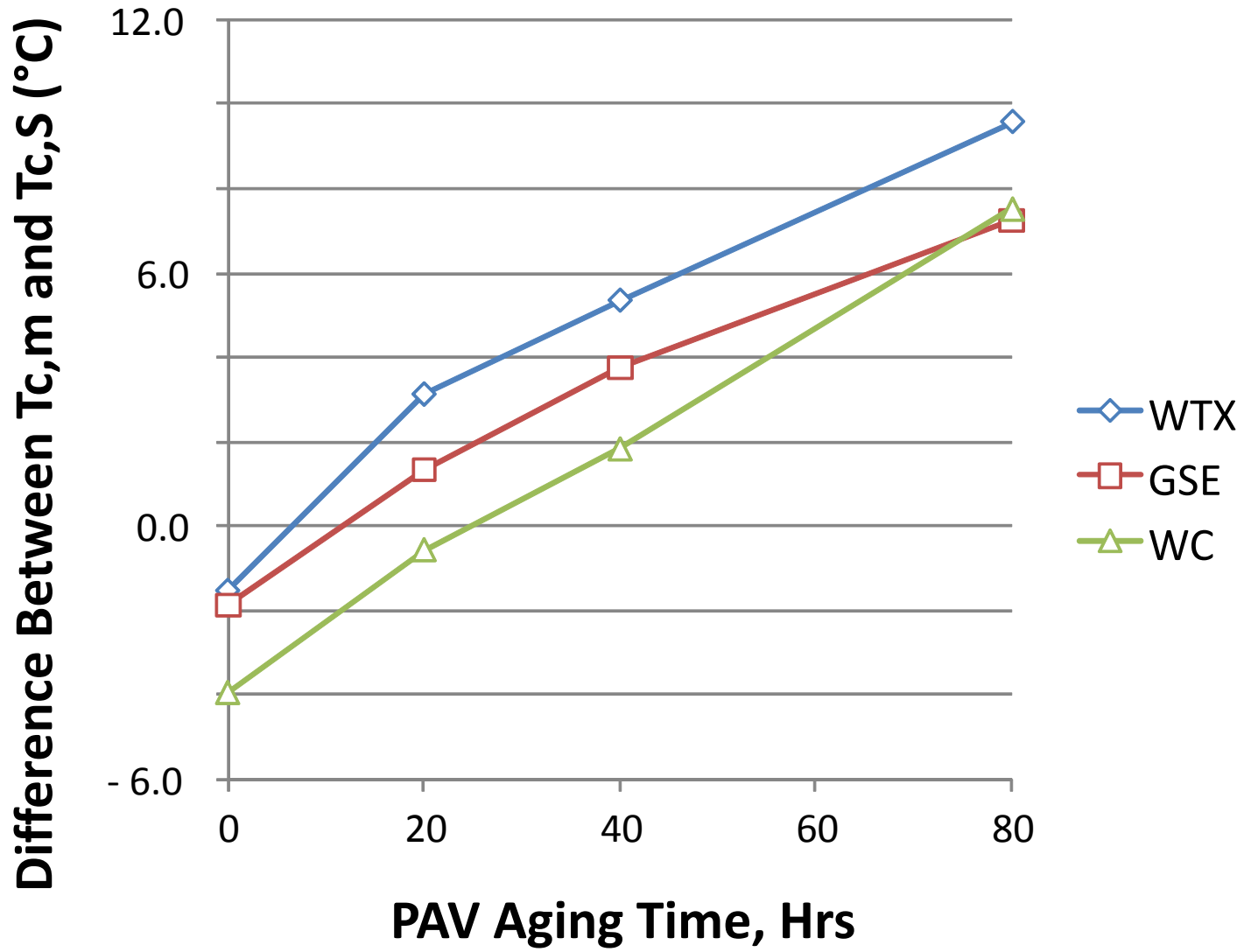
- Lab Study
 - Asphalt Binder Study
 - Various aged conditions
 - Asphalt Mixture Study
 - Various aged conditions
- Field Study
 - Limited validation of lab findings
 - Asphalt binder and mixture tests

- Three asphalt binders representing different expected aging characteristics
 - Selected based upon the relative relationships between low temperature stiffness (S) and relaxation (m-value)
 - West Texas Sour (PG 64-16)
 - 3.1°C m-controlled
 - Gulf Southeast (PG 64-22)
 - 1.3°C m-controlled
 - Western Canadian (PG 64-28)
 - 0.6°C S-controlled

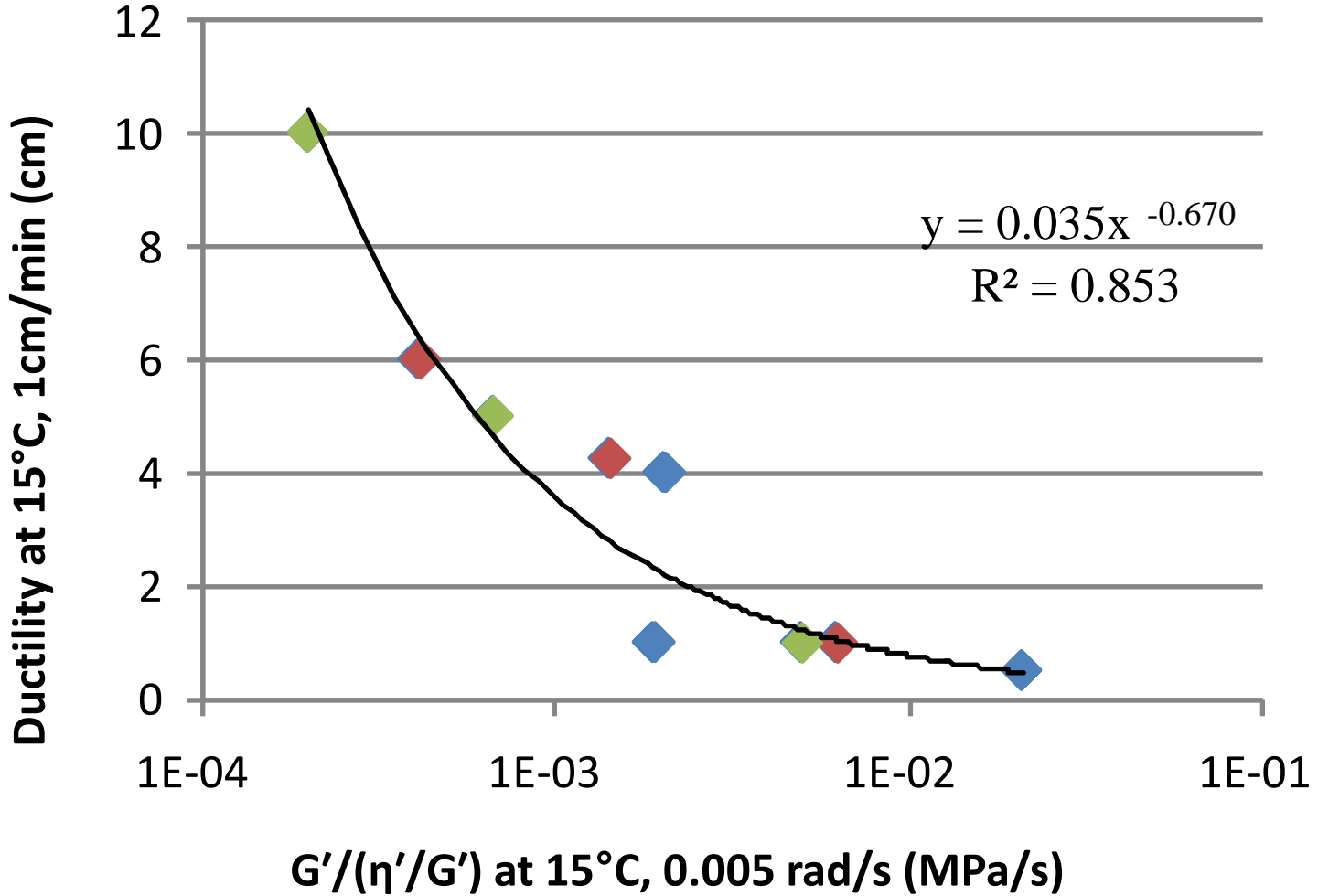
BBR: Gulf-Southeast (GSE)



Effect of PAV Aging Time on ΔT_c

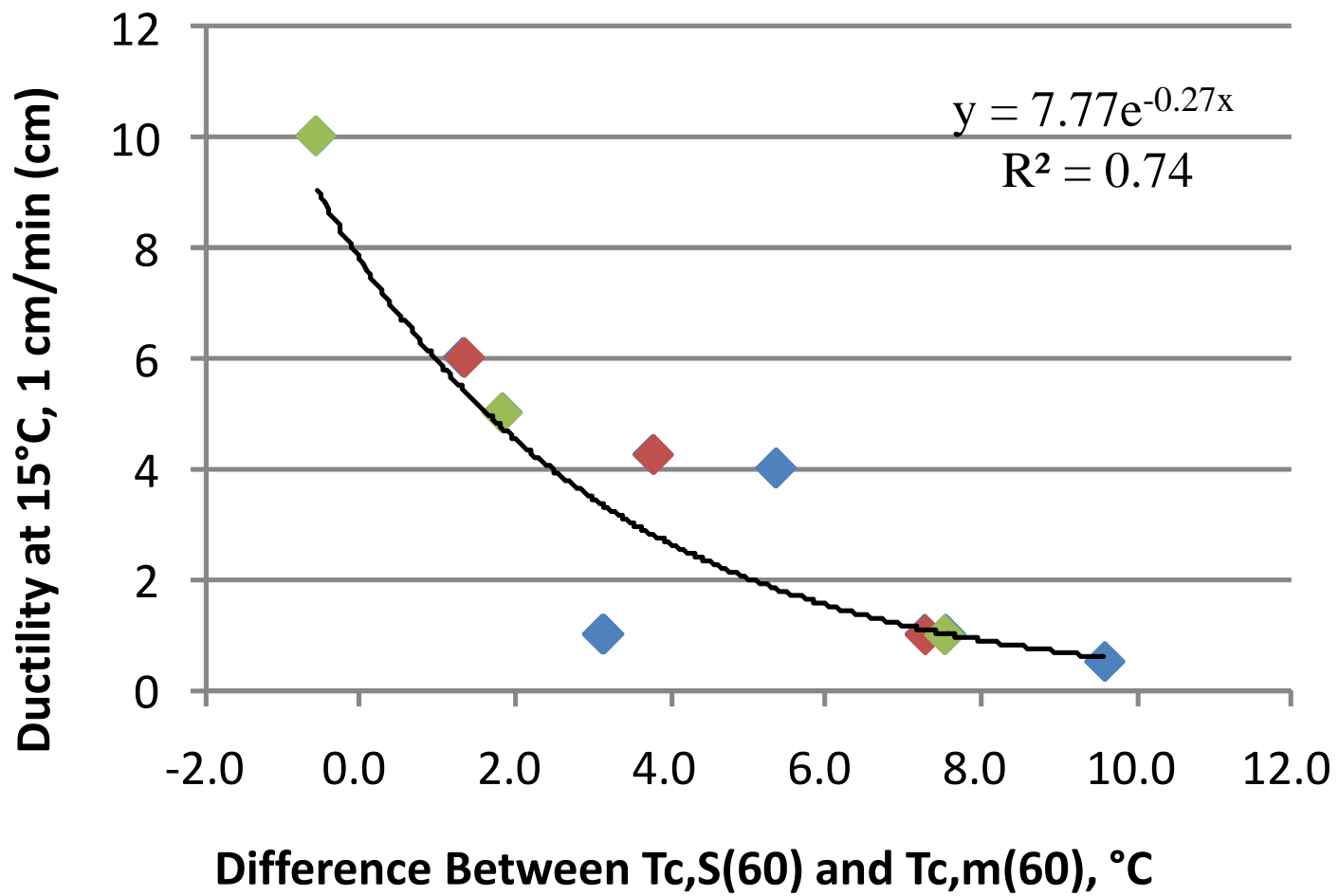


Mastercurve Procedure



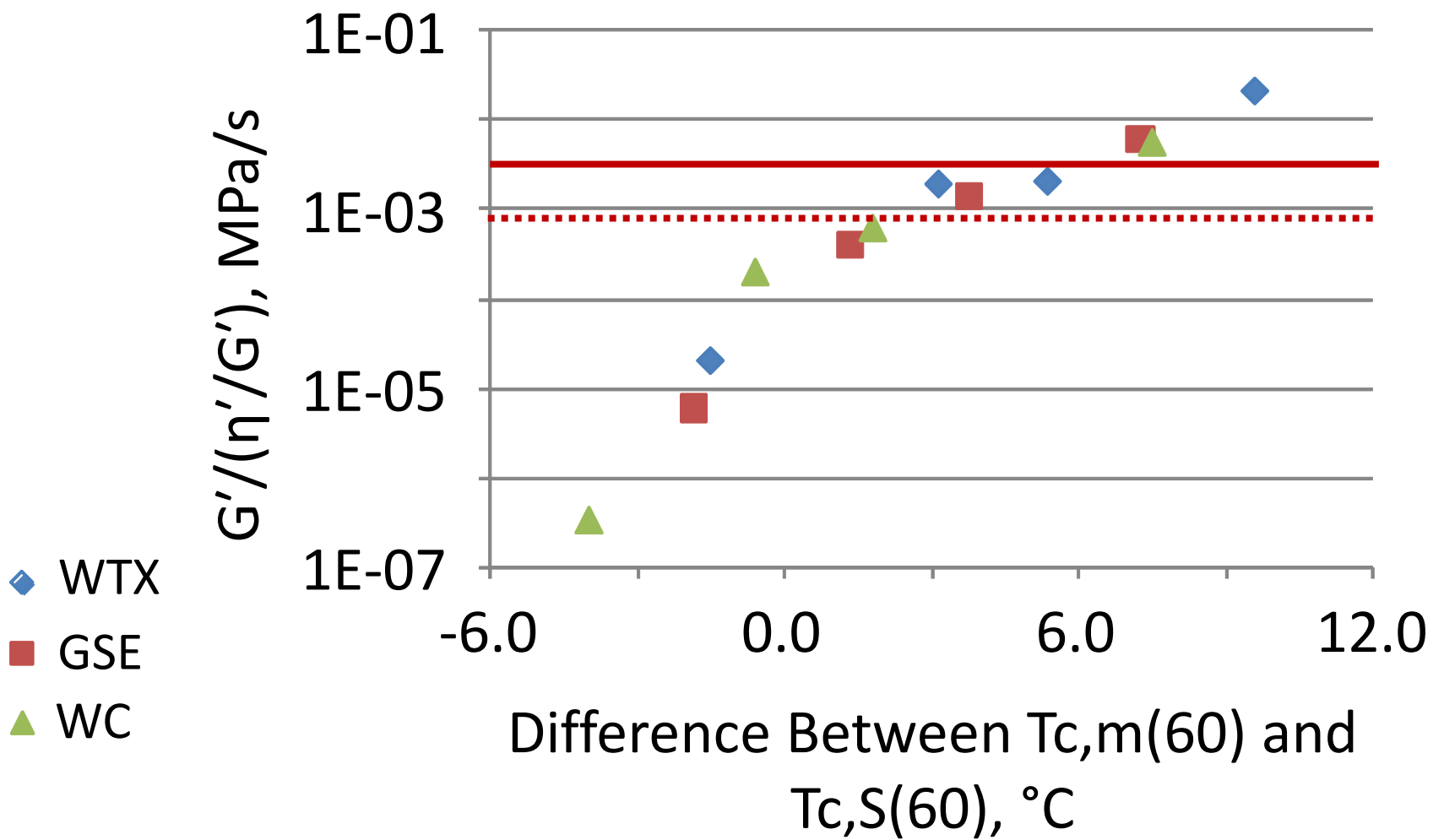
◆ WTX ◆ GSE ◆ WC

Relationship between ΔT_c and Ductility

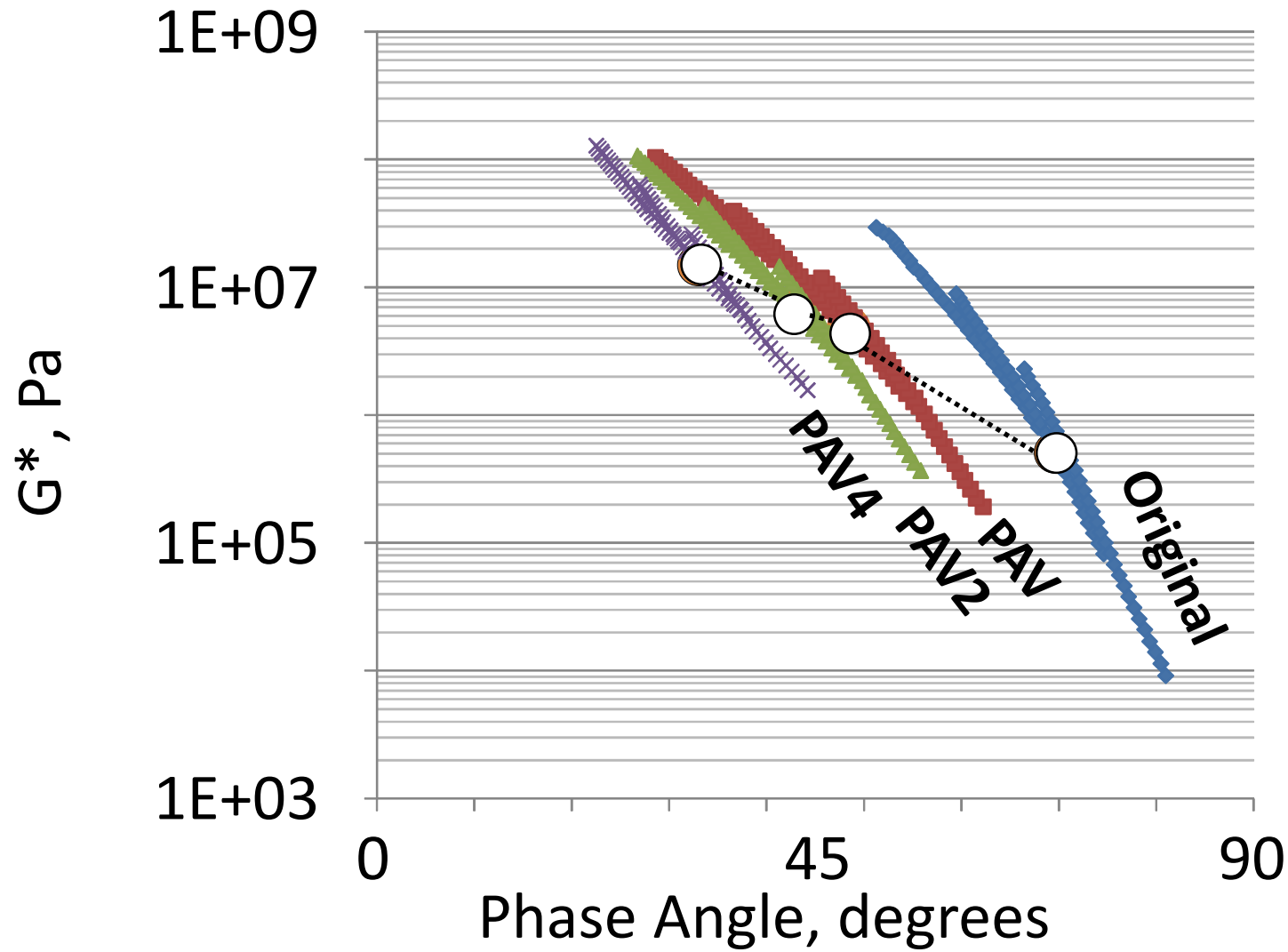


◆ WTX ◆ GSE ◆ WC

Relationship between $G'/(η'/G')$ and $ΔT_c$



Effect of Aging

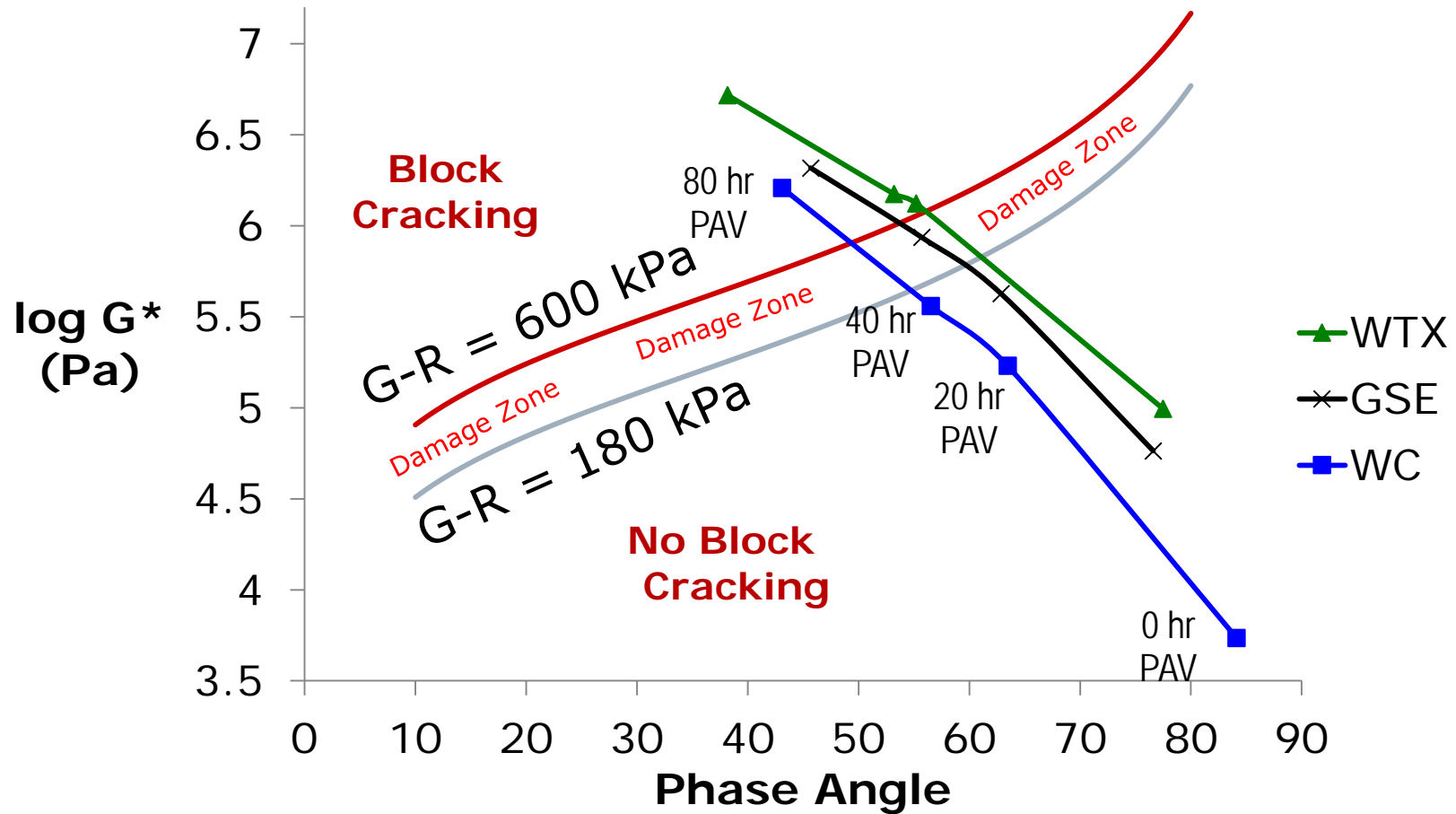


$$G' / \left(\frac{\eta'}{G'}\right) = G^* \omega ((\cos \delta)^2 / \sin \delta)$$

	Ductility 15C, 1 cm/min	Glover-Rowe 0.005 rad/sec
Damage Onset: Early Raveling	5	180 kPa
Damage Visible: Surface cracking	3	600 kPa

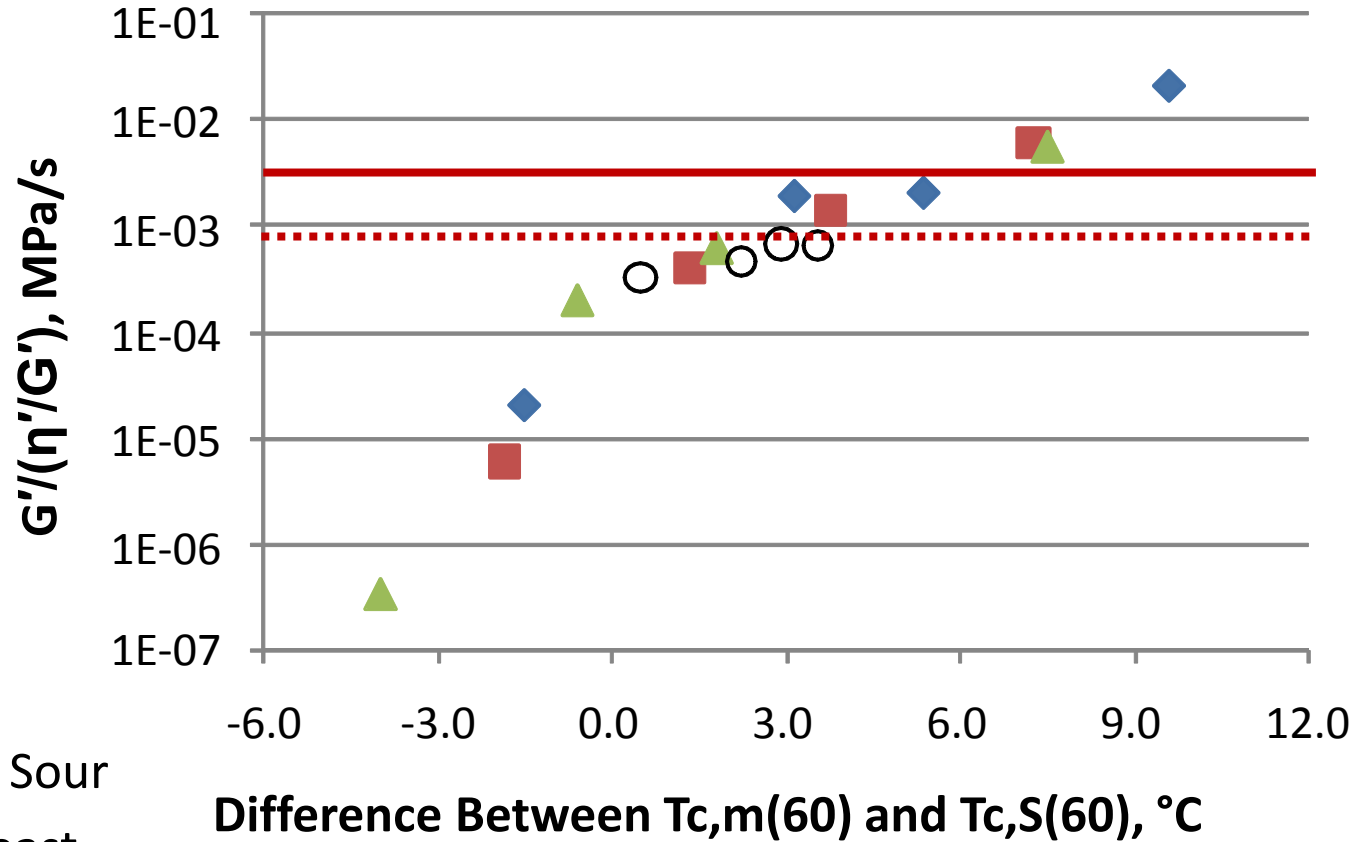
Rowe: Prepared Discussion to M. Anderson paper - AAPT 2011

Glover-Rowe Plot in Black Space: DSR on Aged Binders (15°C; 0.005 rad/s)



- Three general aviation (GA) airport projects representing four in-service pavements
 - Roundup (Montana)
 - Upper layer representing the new pavement (Roundup Top)
 - Lower layer representing the older pavement (Roundup Bottom)
 - Clayton (New Mexico)
 - Some low-severity longitudinal cracking and raveling
 - Conchas Lake (New Mexico)
 - Some low-to-moderate severity raveling was identified over most of the paved area
 - Pavement surface appeared slightly oxidized

Relationship between $G'/(η'/G')$ and $ΔT_c$ (with Field Cores)



- ◆ West Texas Sour
- Gulf Southeast
- ▲ Western Canadian
- Recovered

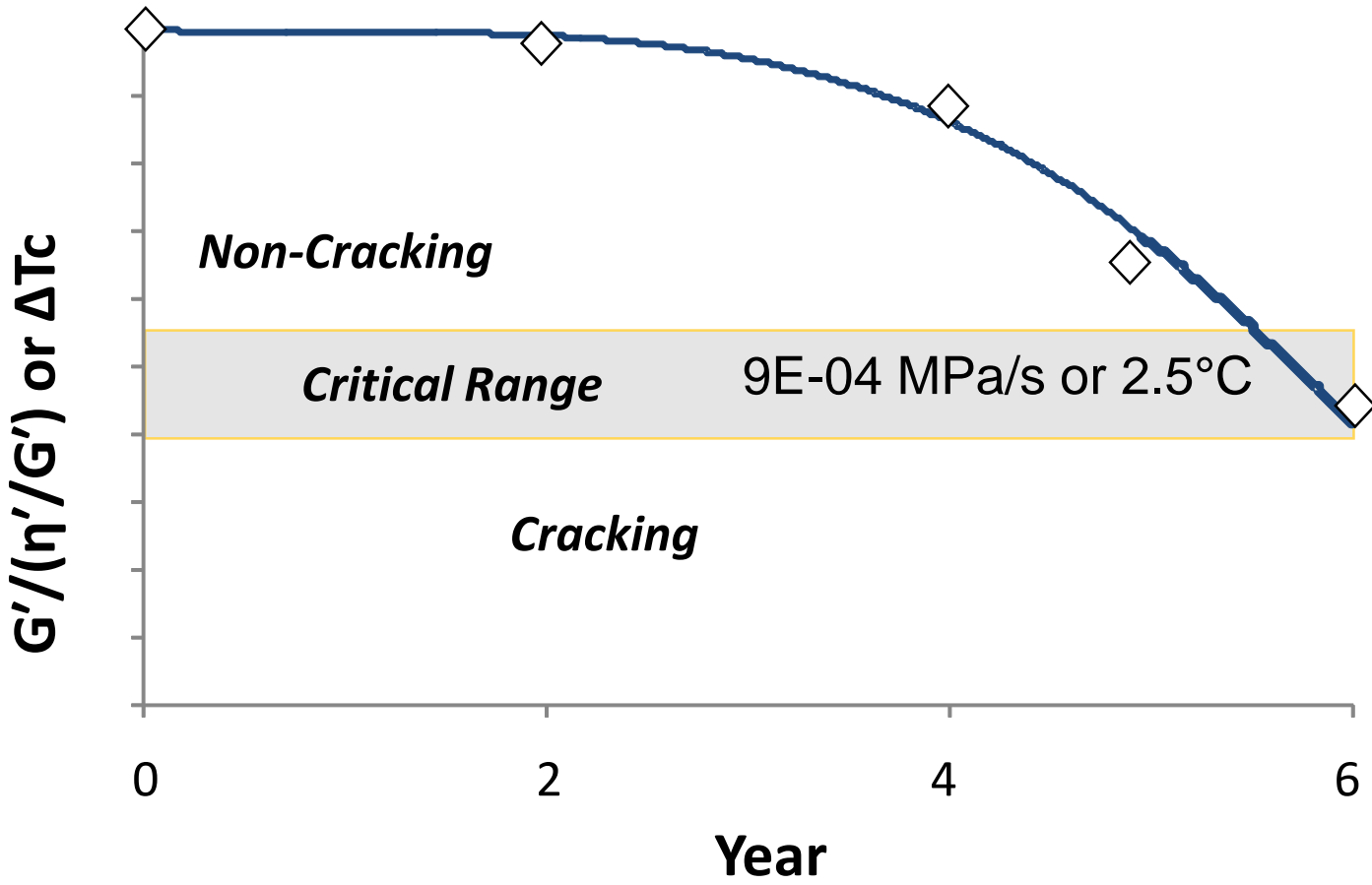
- Past research
 - Some relationship between ductility (conducted at an intermediate temperature) and the durability of an asphalt pavement
 - Texas A&M research validated through identification of DSR parameter, $G' / (\eta' / G')$, at 15°C and 0.005 rad/s

- Current research
 - Confirmed relationship of Texas A&M DSR parameter, $G' / (\eta' / G')$, at 15°C and 0.005 rad/s, to ductility
 - Identified similar parameter through BBR testing, ΔT_c , which quantifies the difference in continuous grade temperature for stiffness and relaxation properties
 - Parameters appear to quantify the loss of relaxation properties as an asphalt binder ages

- Field Studies

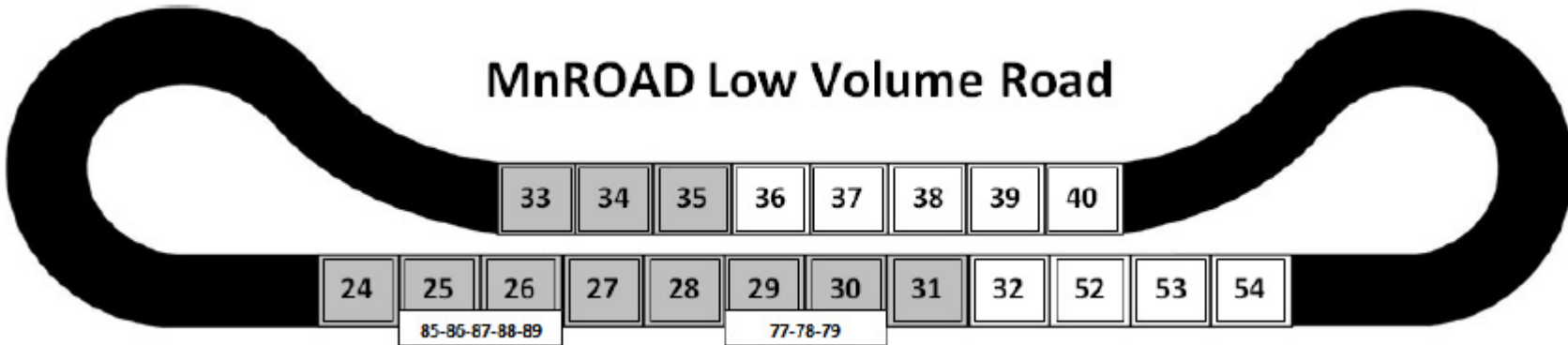
- Four sections from three GA pavements in Montana and New Mexico
- Findings generally matched the lab studies, with the newer pavements having values of $G'/(η'/G')$ and $ΔT_c$ that indicated less aging and more flexibility than the older pavements

Concept

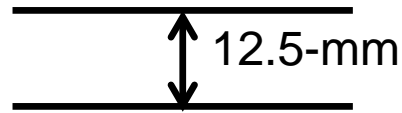
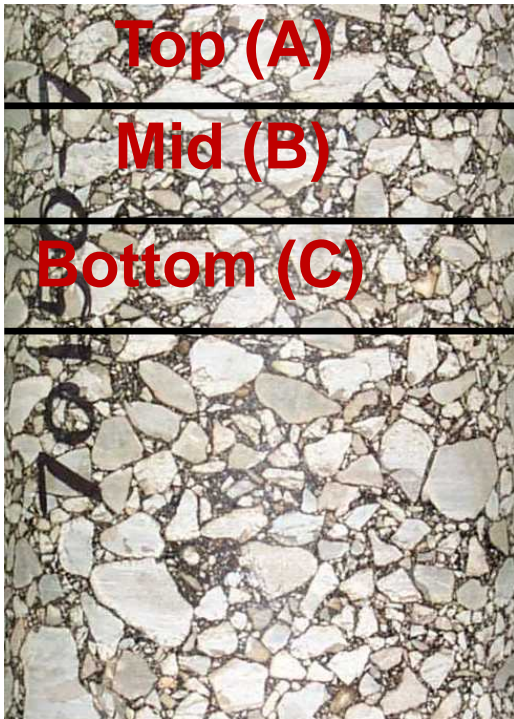


- Laboratory and Field Evaluation of MnROAD and Other Test Sections
 - Critical fracture parameters monitored throughout the life of the pavement
 - Appropriate remedial action can be taken as the critical limit is approached
 - Simple tests to be used for field monitoring purposes
 - physical properties from simple tests correlated to crack predictions from DC(t) or other more sophisticated fracture tests.

MnROAD Low Volume Road



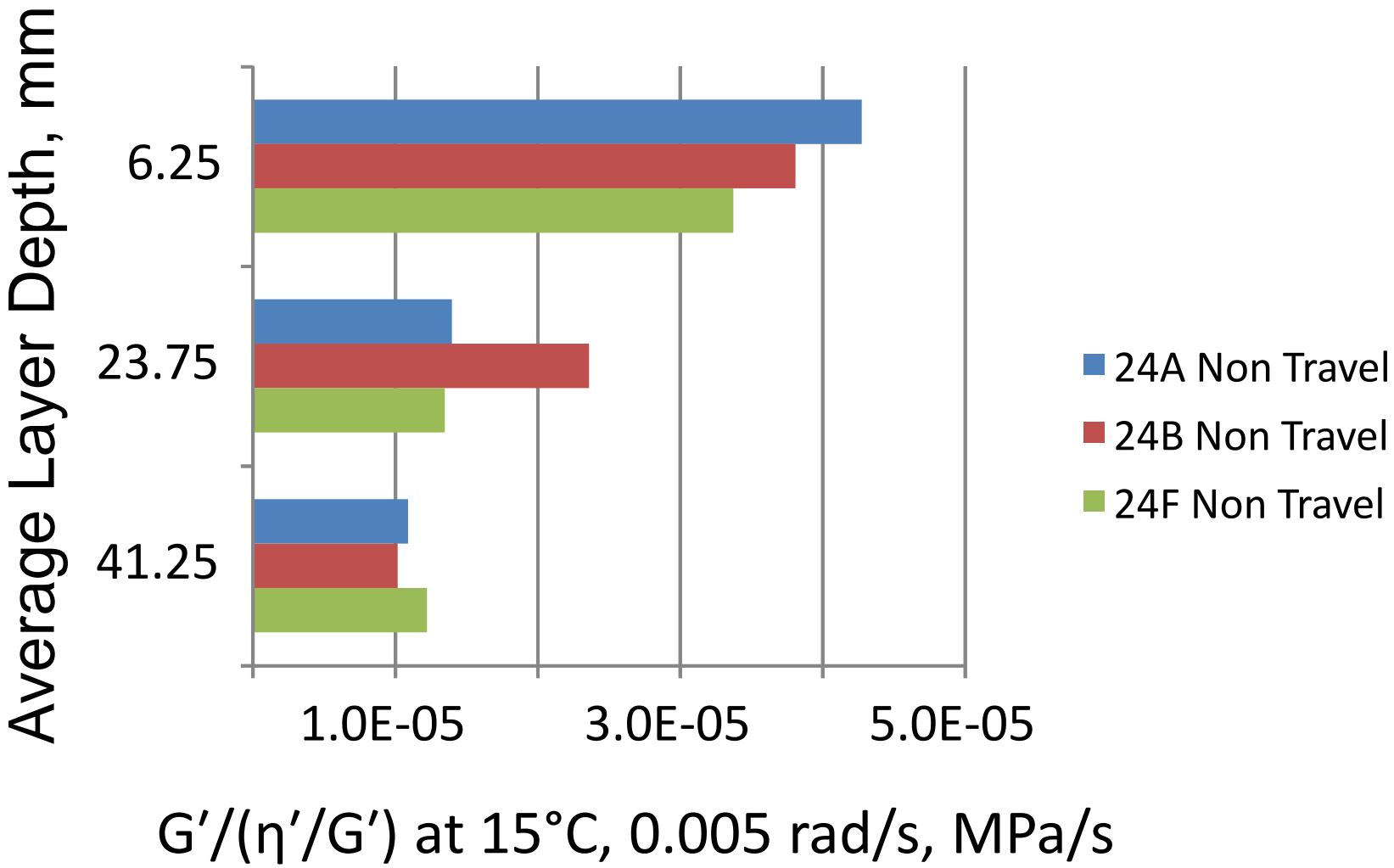
24	33	34	35	27	28
3" 58-34	4" 58-34 PPA	4" 58-34 SBS+PPA	4" 58-34 SBS	2" 52-34	2" 52-34
4" Class 6				2" 58-34	2" 58-34
Sand	12" Class 6	12" Class 6	12" Class 6	6" Class 5	6" Class 5
100' Fog Seals 2008 2009 2010 2011 2012				G CBD	
	Clay	Clay	Clay	2009 Chip Seal	
				7" Clay Borrow	7" Clay Borrow
				Clay	Clay
Oct 08	Sep 07	Sep 07	Sep 07	Aug 06	Aug 06
Current	Current	Current	Current	Current	Current

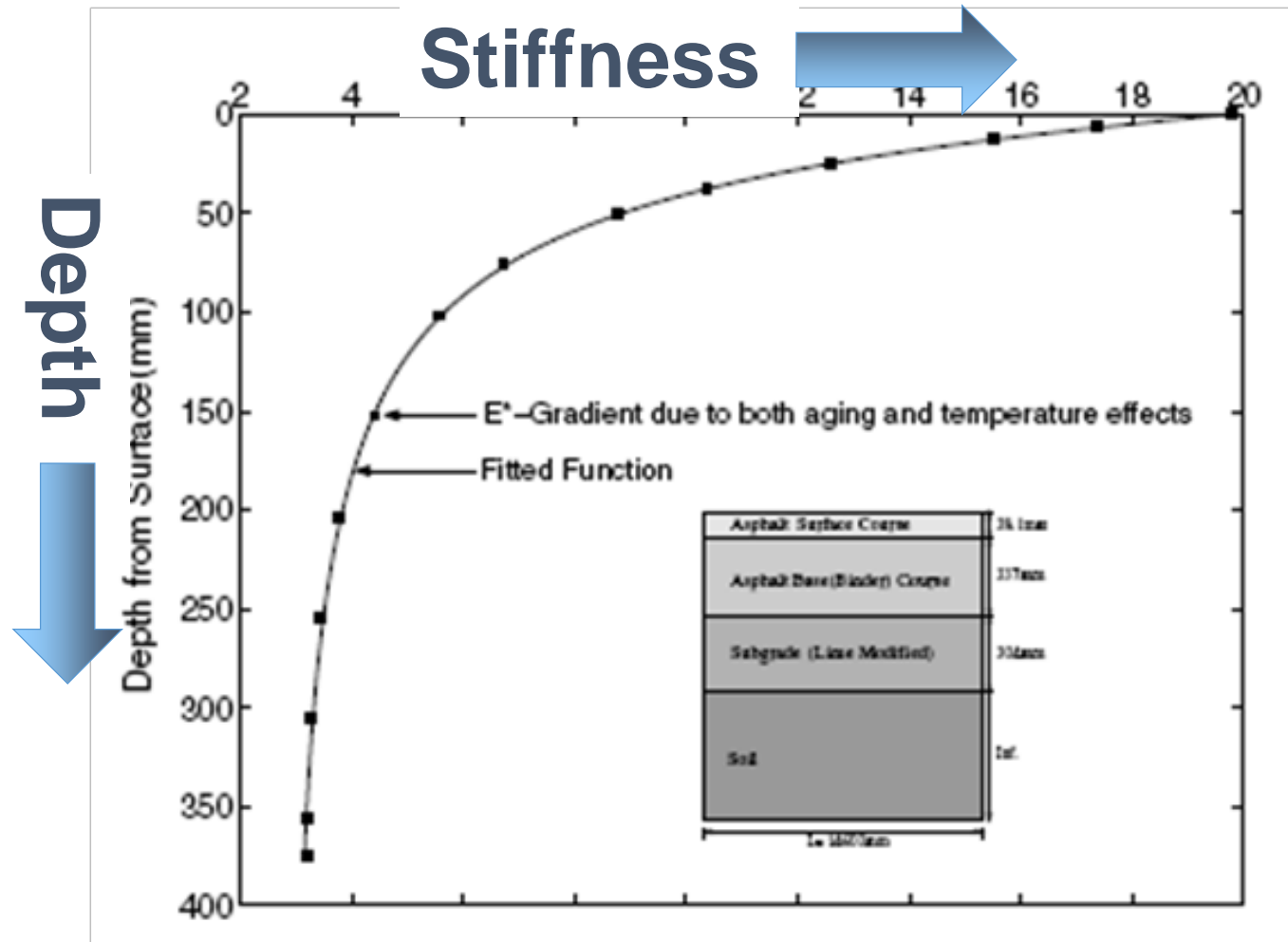


- Extraction/Recovery
 - Centrifuge extraction using toluene/ethanol
 - Recovery using Rotavapor
- 2 Cores (150-mm diameter x 12.5-mm thickness)
 - ~50 grams asphalt

- Each Layer
 - DSR Temperature-Frequency Sweep
 - Three temperatures (5, 15, 25°C) using 8-mm plates
 - Rheological mastercurves for modulus (G^*) and phase angle (δ)
 - BBR
 - T_c determined to the nearest 0.1°C for S(60) and m(60)
 - Difference in T_c (ΔT_c)

MnROAD Cell 24: Effect of Layer Depth

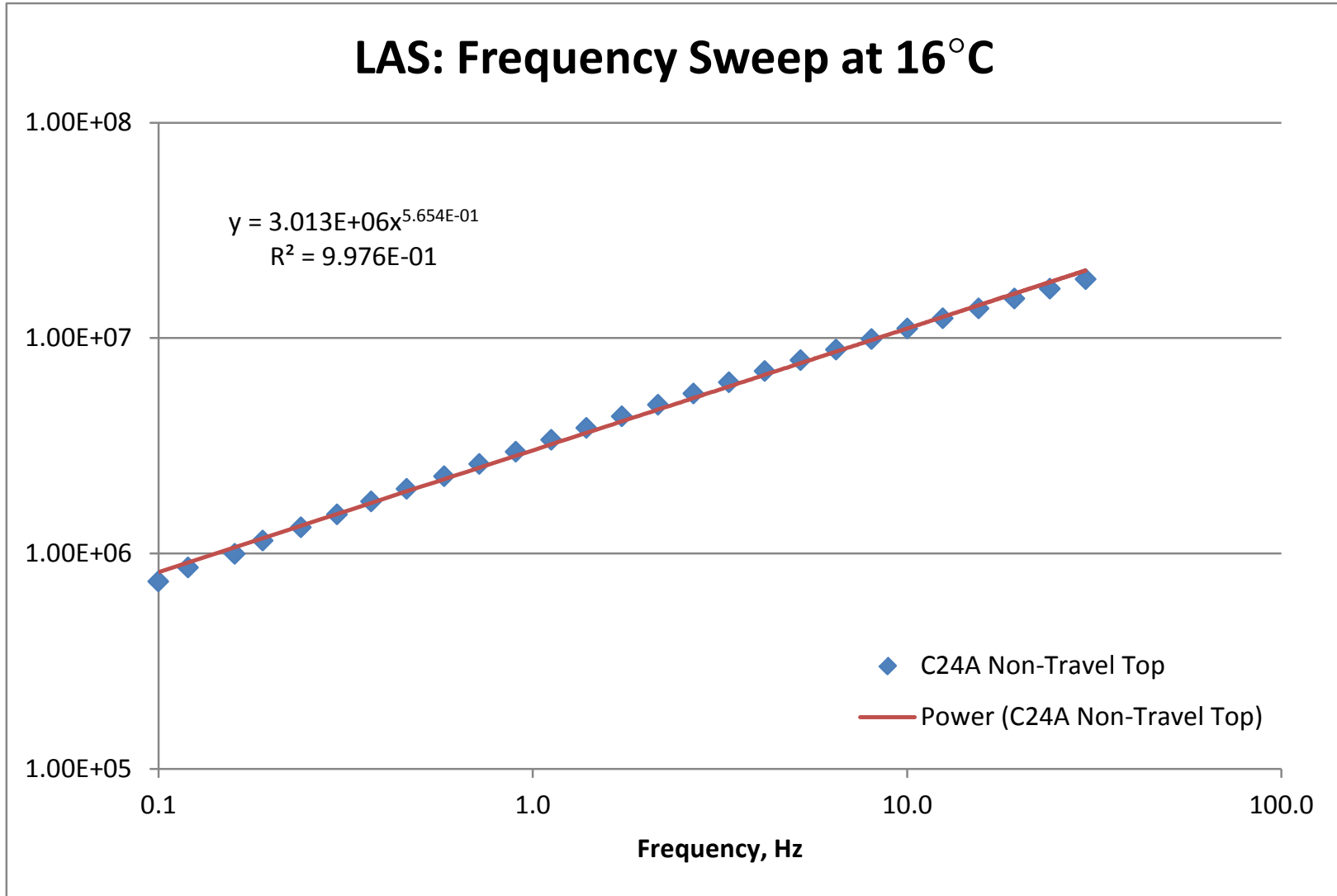




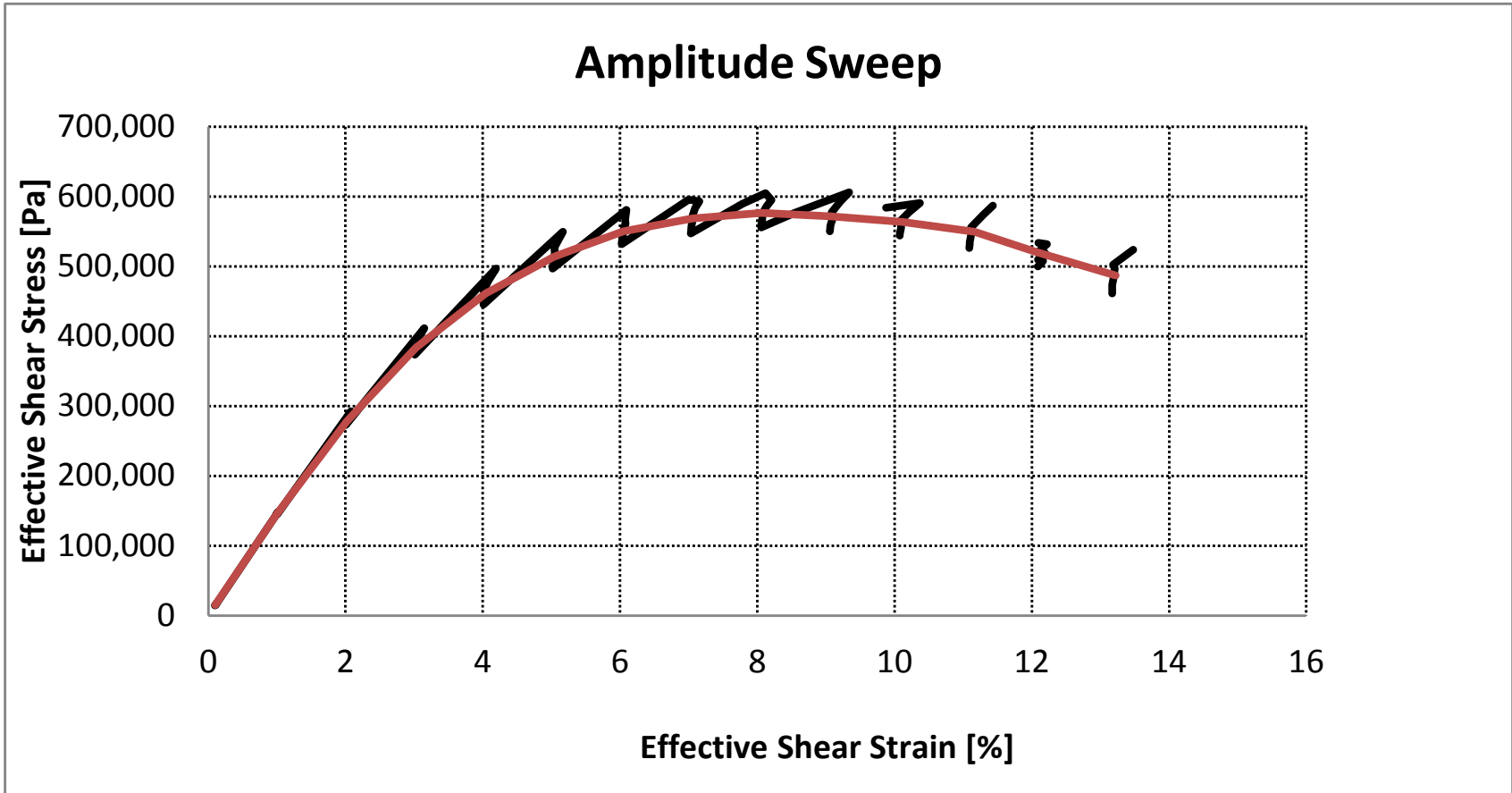
- Linear Amplitude Sweep (LAS) Test
 - DSR Test
 - Frequency Sweep (0.1 – 30 Hz)
 - Continuous Oscillation at 10 Hz with Linearly-Increasing Strain from 0.1 to 30%
 - Viscoelastic Continuum Damage (VECD) analysis to get reduction in $G^* \sin \delta$
 - Cycles to failure as a function of strain

$$N_f = A\gamma^B$$

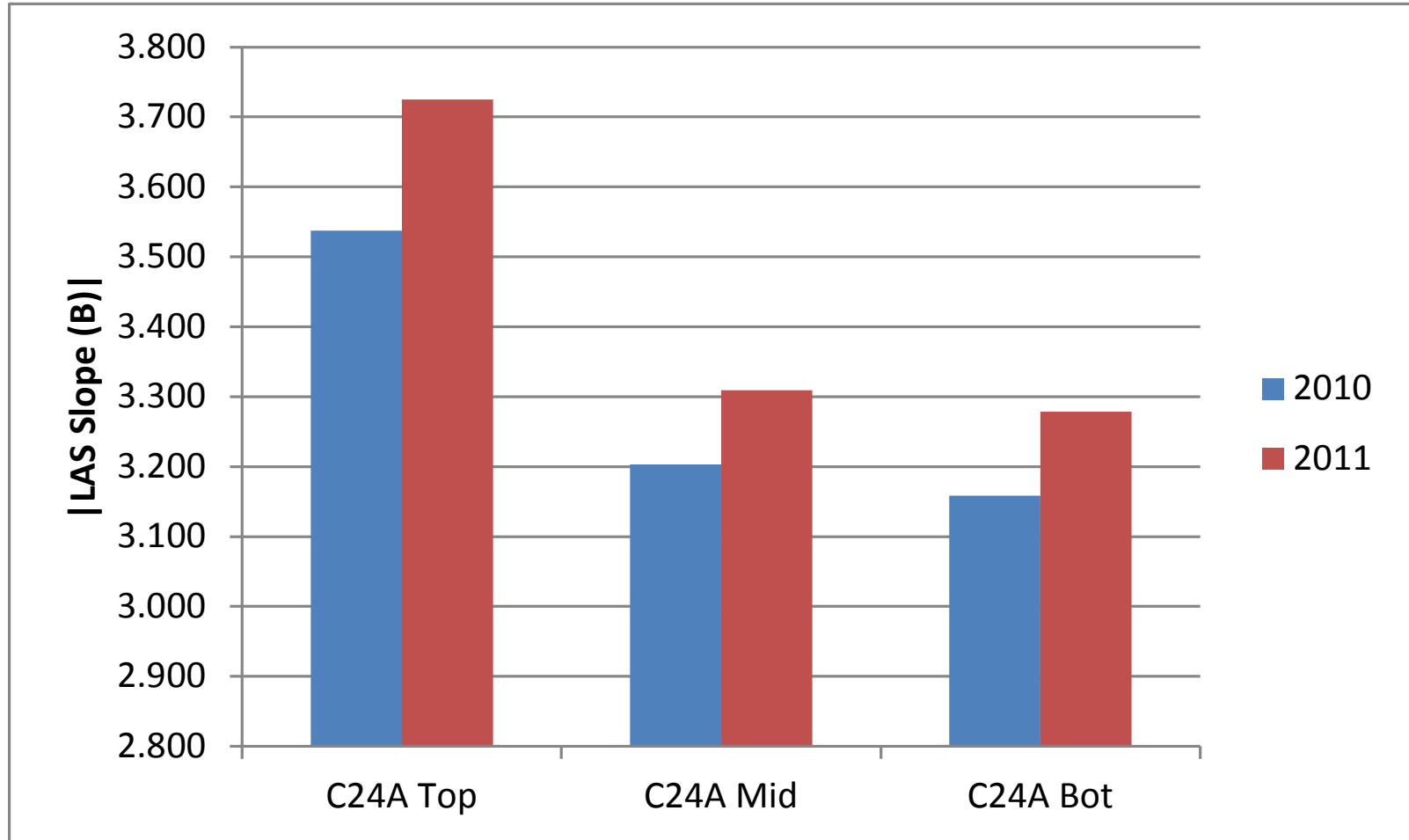
LAS Frequency Sweep



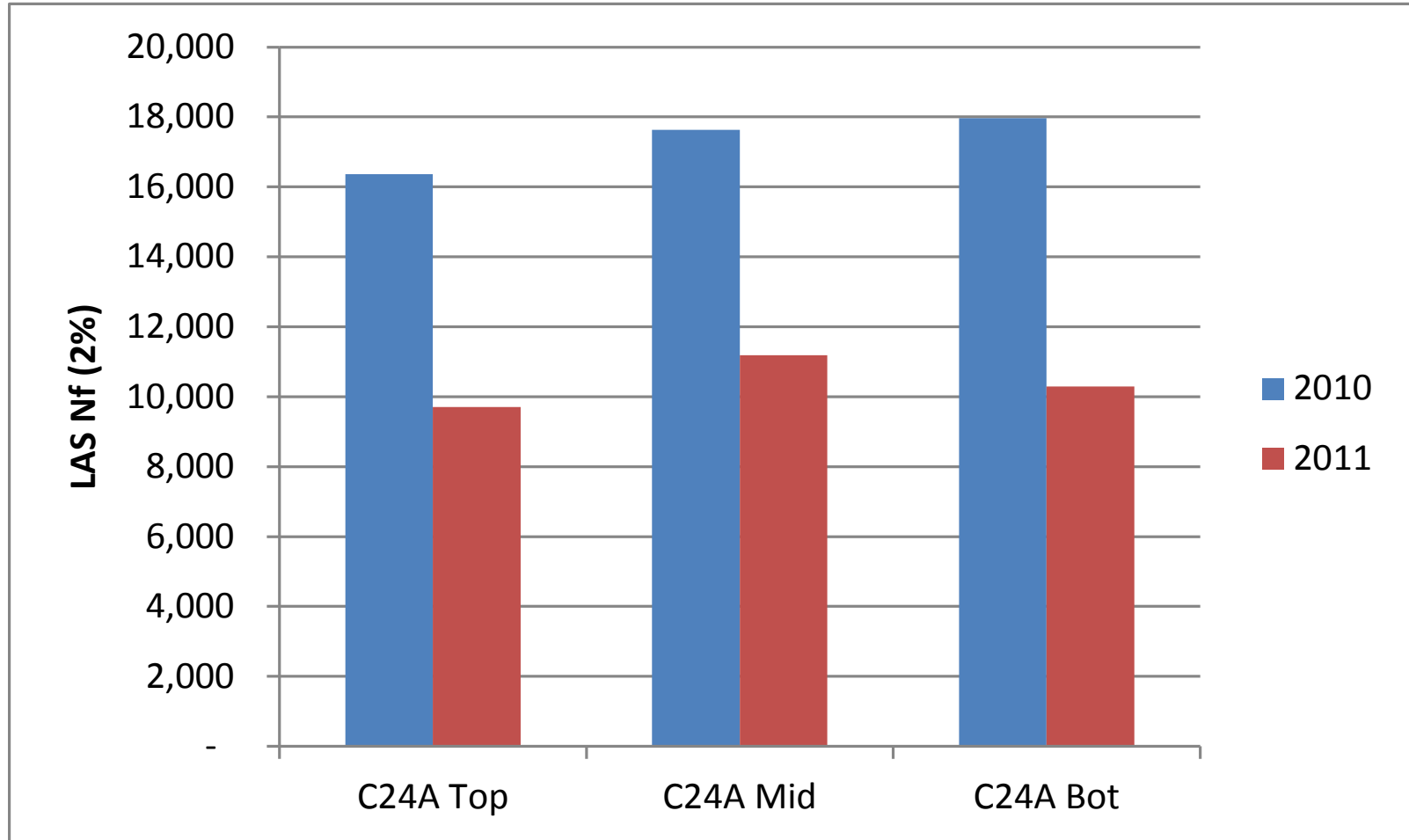
LAS Strain Sweep



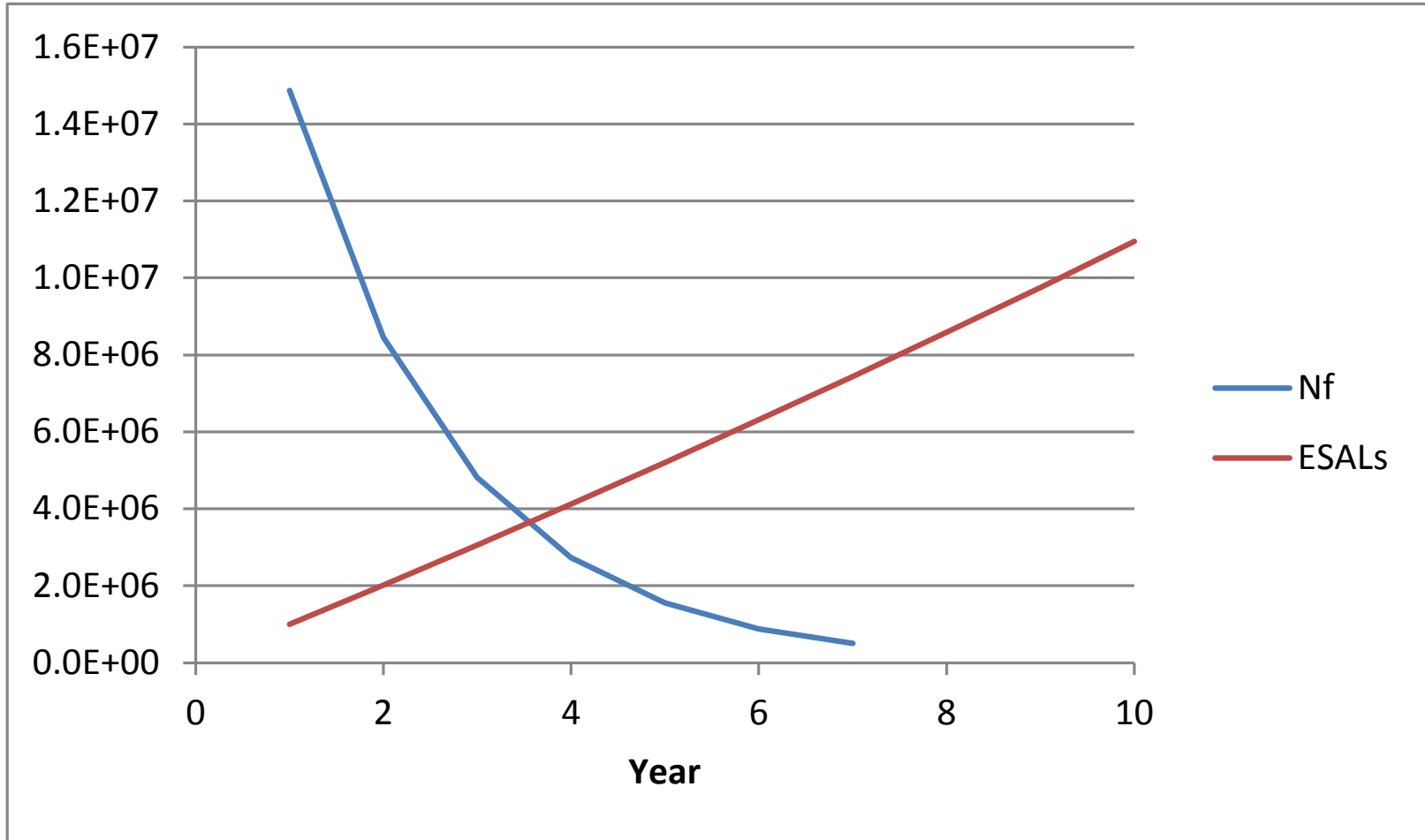
Aging as a Function of Depth and Time: LAS Slope (B)



Aging as a Function of Depth and Time: LAS N_f (2%)



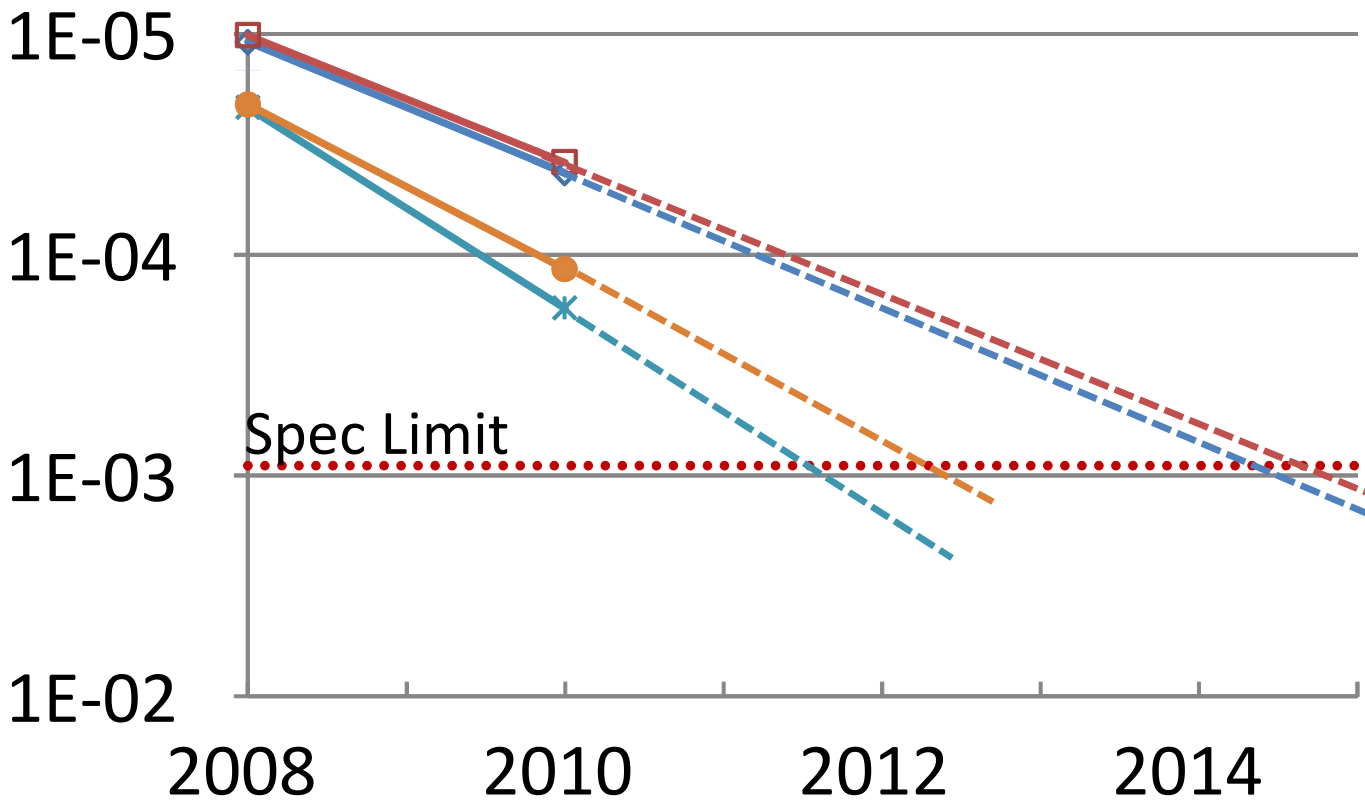
Effect of Aging (Conceptual)




MnROAD Cell 24: Aging Profile



$G'/(η'/G')$ at 15°C and 0.005 rad/s, MPa/s



- Effects of Aging
 - Increase stiffness
 - Decrease flexibility
- 
- Surface Cracking



Thanks!

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