

Fatigue Endurance Limits for Perpetual Pavements

By

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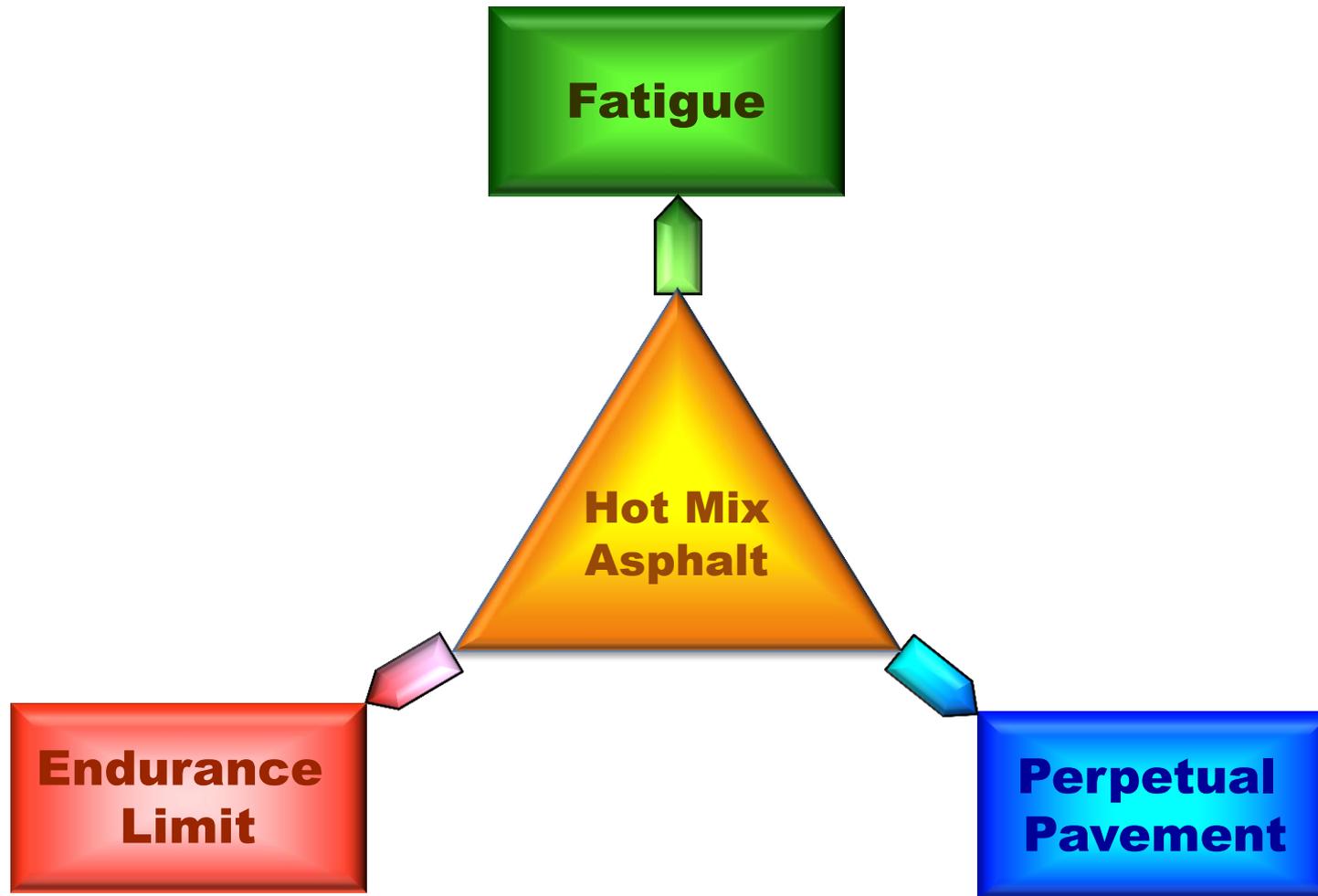
Outline

- Background
- Research Statement and Objectives
- Testing Plan and Design of Experiment
- Endurance Limit (EL) Algorithm Development
- Development of SR Models
- Comparison of EL from Uniaxial and Beam Fatigue
- Incorporating EL Methodology into AASHTOWare-ME
- Conclusions, and Recommendations

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Background



HMA Fatigue Damage/Cracking

- **Definition:** A load associated damage due to repeated traffic loading.



- **Description:** Three different stages



Early Stage



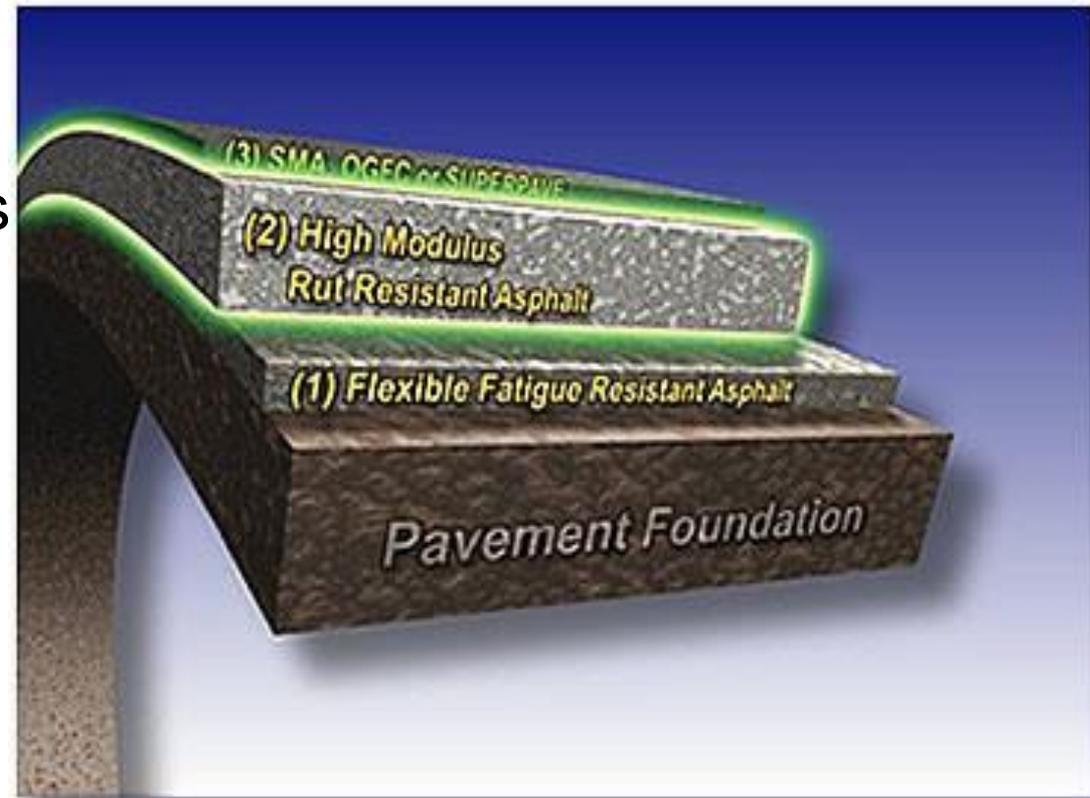
Intermediate Stage



Final Stage

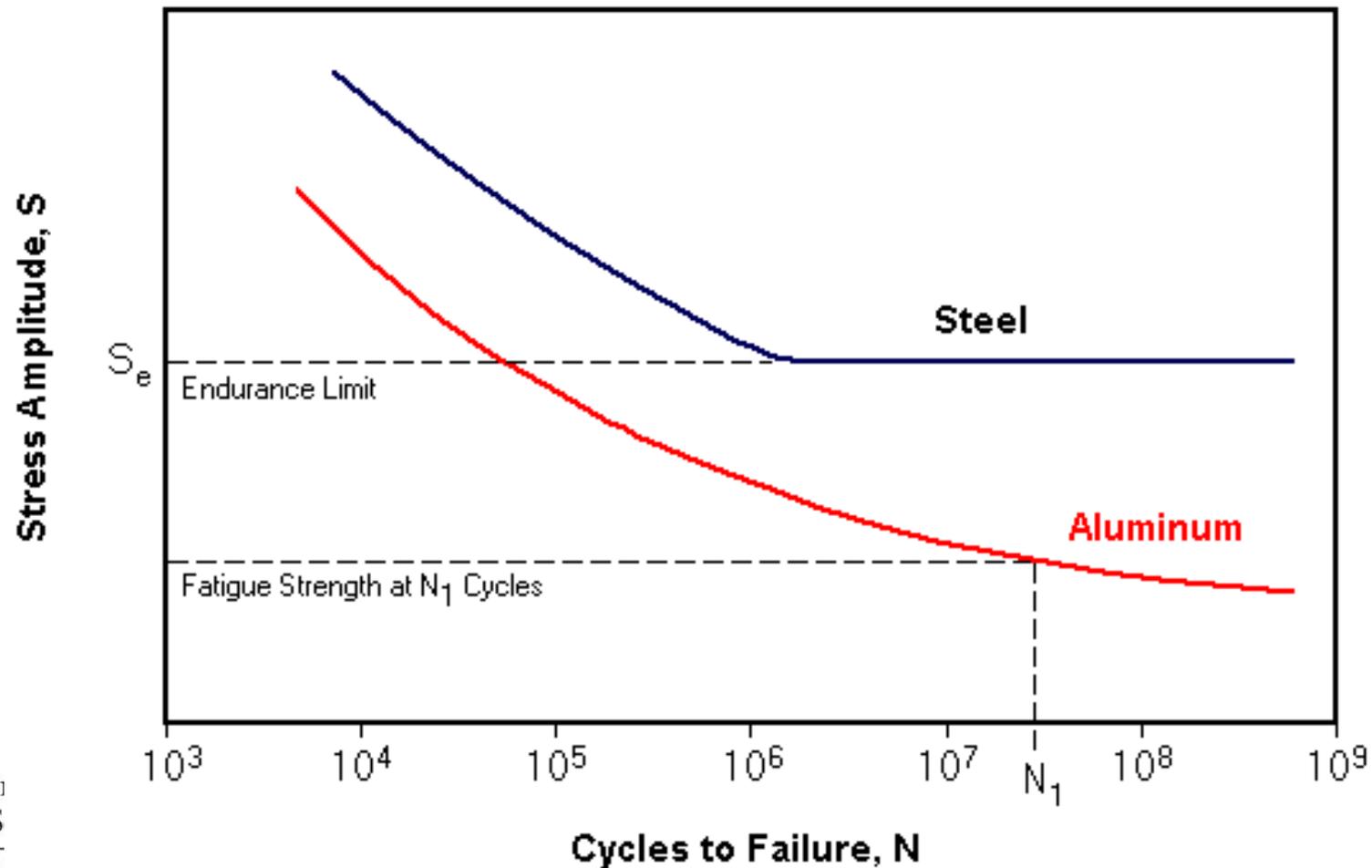
Perpetual Pavements

- **Definition:** Term used to describe a long lasting HMA pavements.
- At least 50 years
- Full depth asphalt, 1960s
- Three HMA layer system
- Increases pavement recycling
- Cost savings
- Environmental benefits.

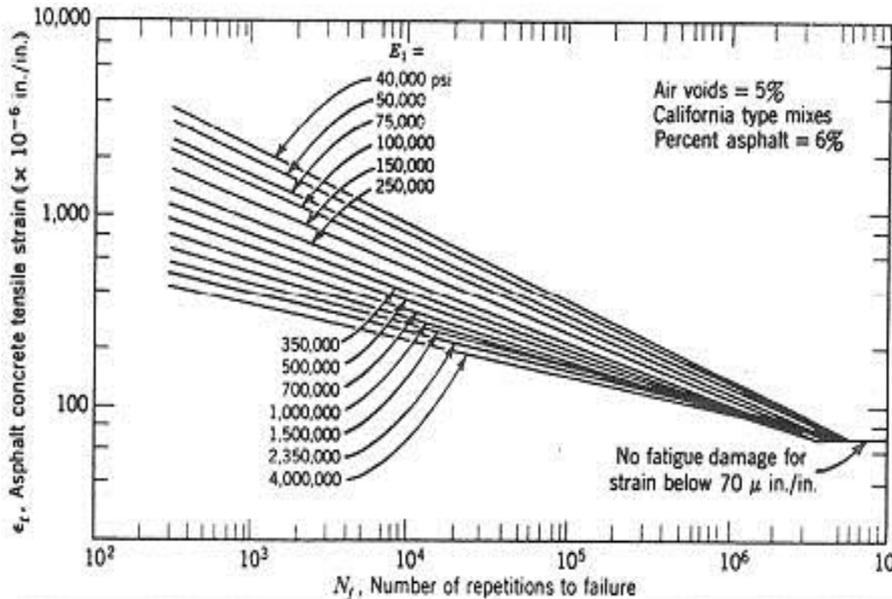


Endurance Limit

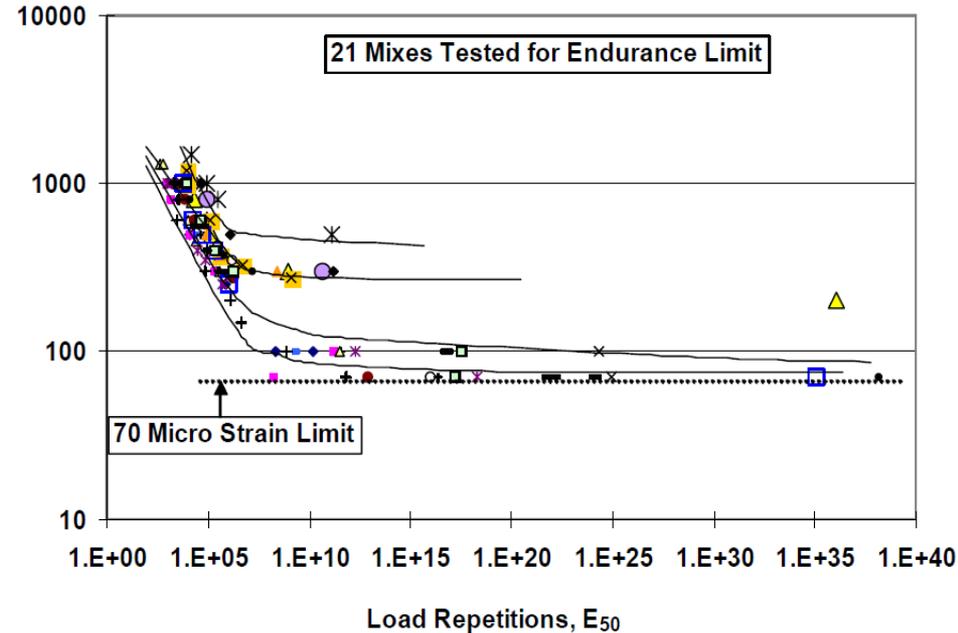
- **Definition:** [Wöhler \(1870\)](#)



Does HMA Exhibit an Endurance Limit?



Monismith et al., 1970

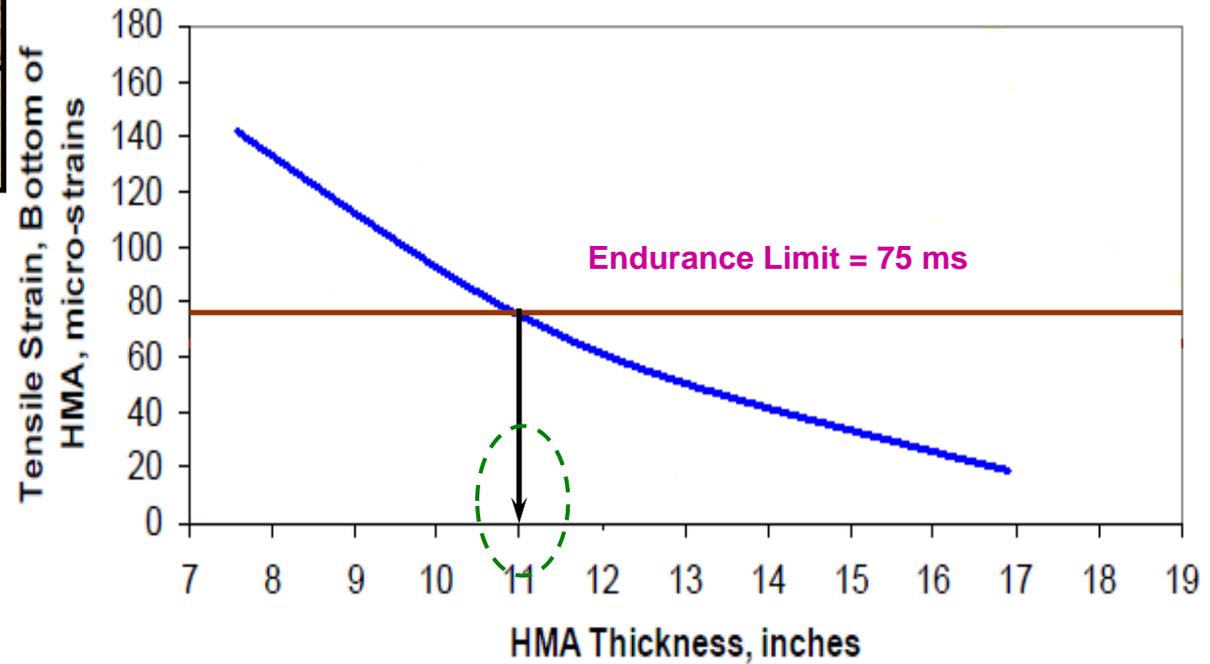
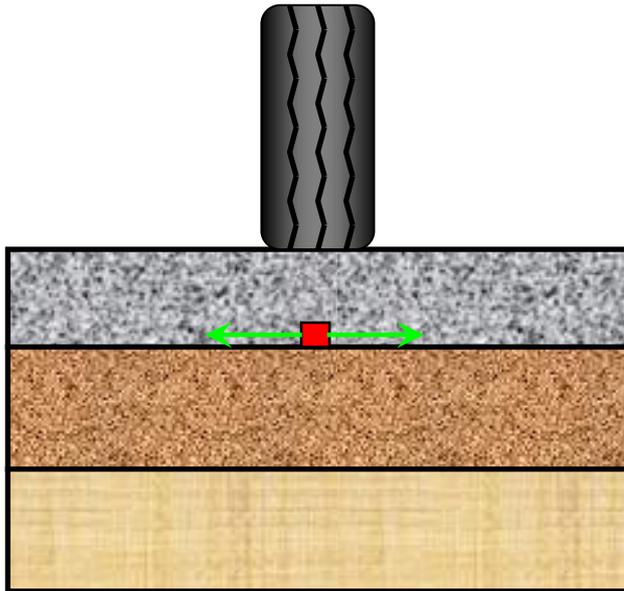


Carpenter et al., 2003

- **HMA EL (Prowell et al., 2009):**

Strain level yields 50 millions load repetitions until failure

Perpetual Pavement Design Concept



Outline

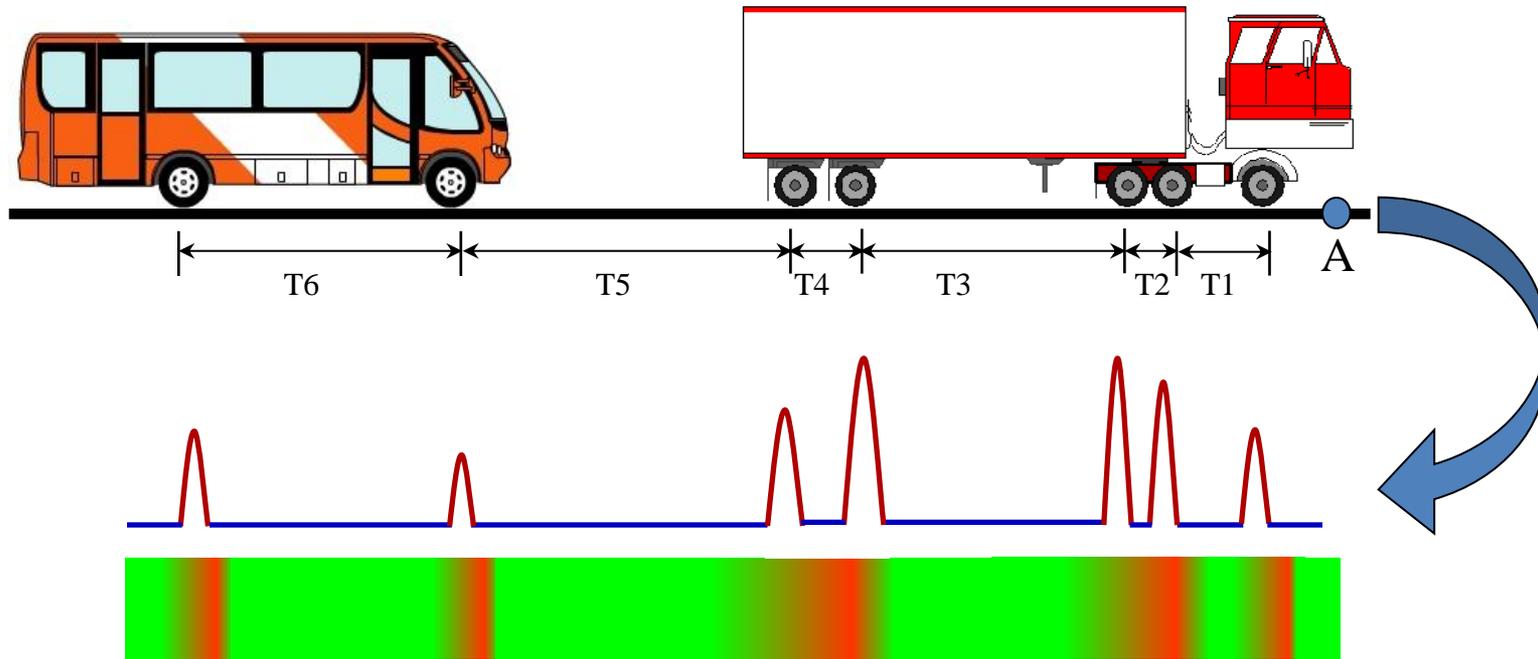
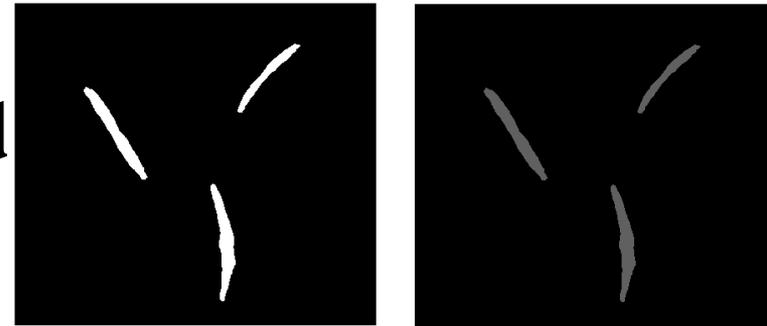
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Research Problem Statement and objectives

- The EL concept has not been totally implemented in AASHTOWare Pavement ME Design software
- No current methodology to consider the effect of the environmental conditions, traffic condition, mix design, and material properties together in the EL calculations
- Develop an algorithm to determine EL that is compatible with the AASHTOWare-ME software

New EL Definition

- EL is a result of a balance of damage caused by loading and healing or damage recovery that occurs during rest periods



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Factors Affecting Fatigue and EL

Factors

Asphalt Content (%)	Binder Grade
Air Voids (%)	Aggregate Type
Temperature (°F)	Filler Percent
Rest Period (seconds)	Aggregate Gradation
Tensile Strain (μs)	Test Type

- ❑ 10 Factors with 3 levels: $3^{10} = 59049$ tests
- ❑ Three replicates: $59049 * 3 = 177147$ tests
- ❑ Assuming average of 10 hours per test
- ❑ Total of **202** years

Selected Factors

Factors	No. of Levels
Asphalt Content, AC (%)	4.2, and 5.2
Air Voids, V_a (%)	4.5, and 9.5
Temperature, T (°F)	40, 70, and 100
Rest Period, RP (seconds)	0, 5, 1, and 10
Tensile Strain, ϵ_t (μ s)	L, M, and H
Binder Type	PG 58-28, 64-24, and 76-16

Test Type



Beam Fatigue Test



Uniaxial Fatigue Test

Binder Type			PG 58-28				PG 64-22				PG 76-16				
Binder Content			4.2		5.2		4.2		5.2		4.2		5.2		
Air Voids (%)			4.5	9.5	4.5	9.5	4.5	9.5	4.5	9.5	4.5	9.5	4.5	9.5	
Temperature, F	Tensile Strain	Rest Period (sec)													
40	L	0					U	U		U					
		1													
		5					U	U	U	U					
		10													
	M	0					U		U	U					
		1						U							
		5						U	U	U					
		10							U						
	H	0								U					
		1								U					
		5					U								
		10													
70	L	0					U	U	U						
		1													
		5					U	U		U					
		10							U						
	M	0					U	U		U					
		1								U					
		5					U	U	U	U					
		10													
	H	0													
		1										U			
		5													
		10													
100	L	0					U		U	U					
		1					U			U					
		5							U	U					
		10													
	M	0							U	U	U				
		1													
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		10													

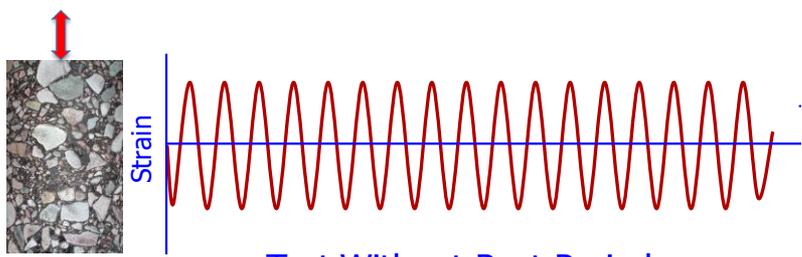
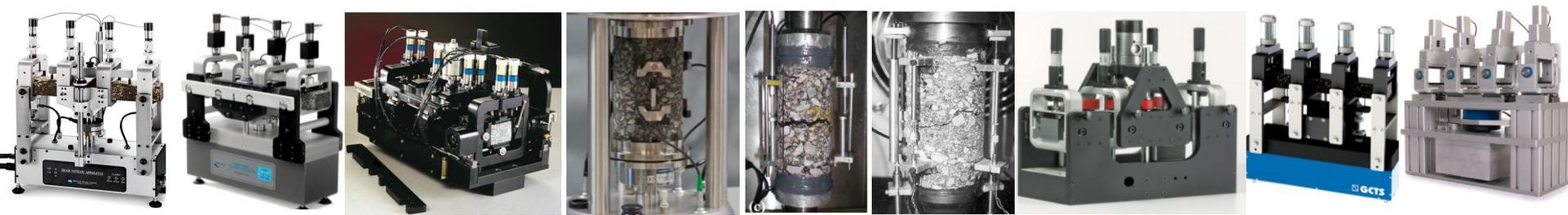
Total Number of Combinations

Beam Fatigue = 190 Uniaxial Fatigue = 51

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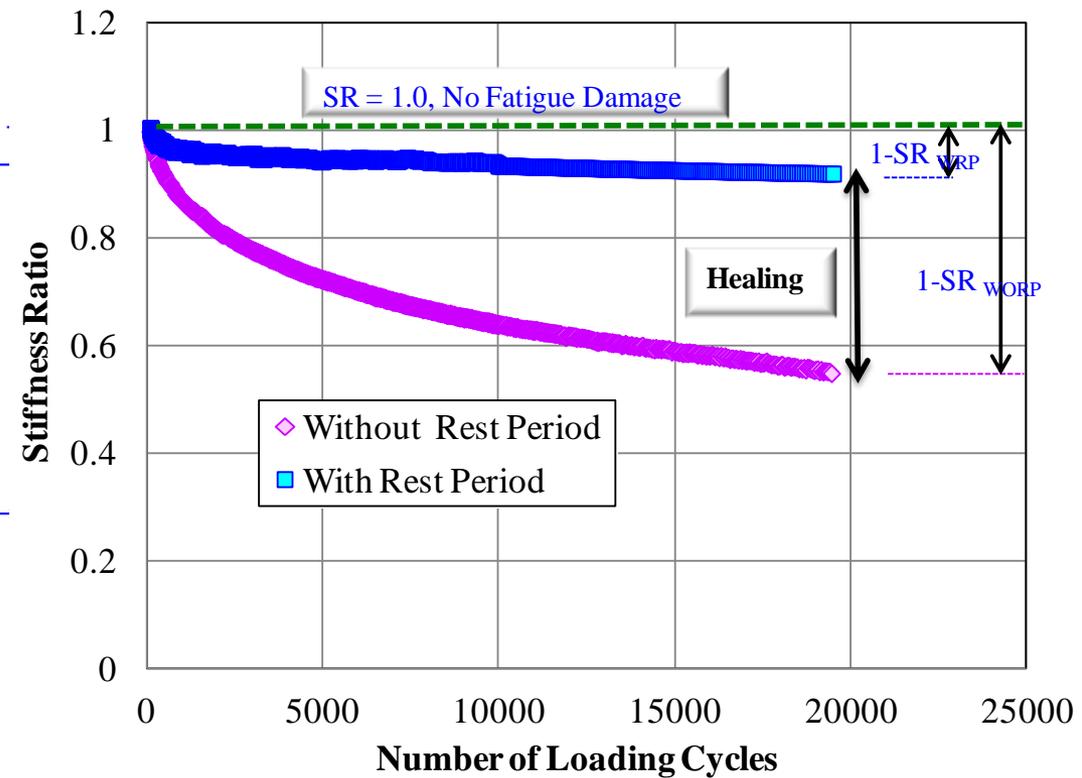
Healing of Micro-cracks



Test Without Rest Periods

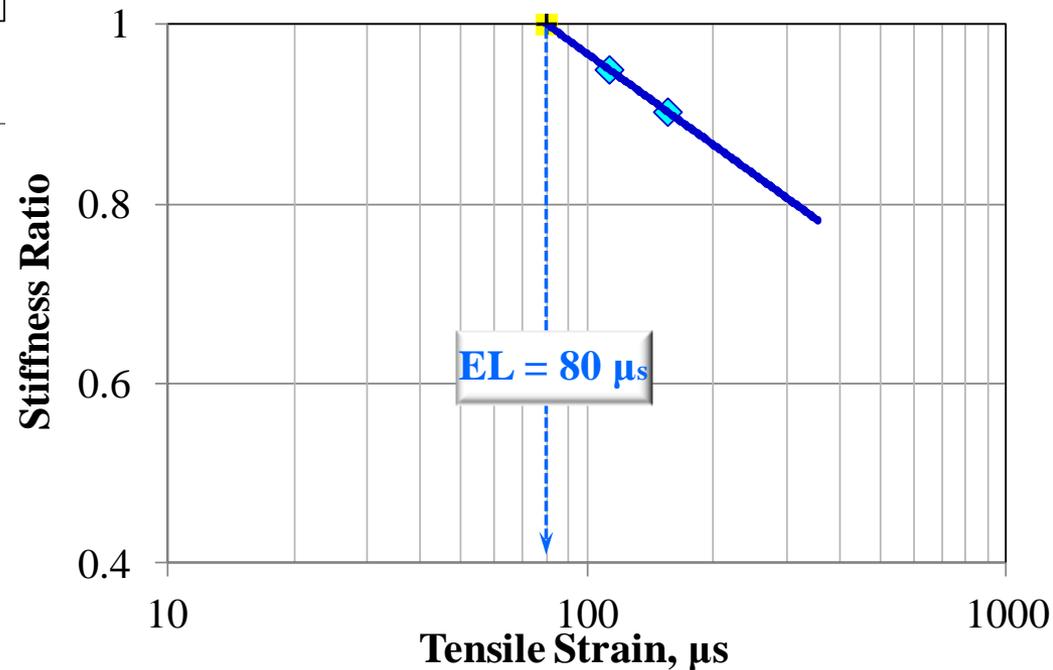
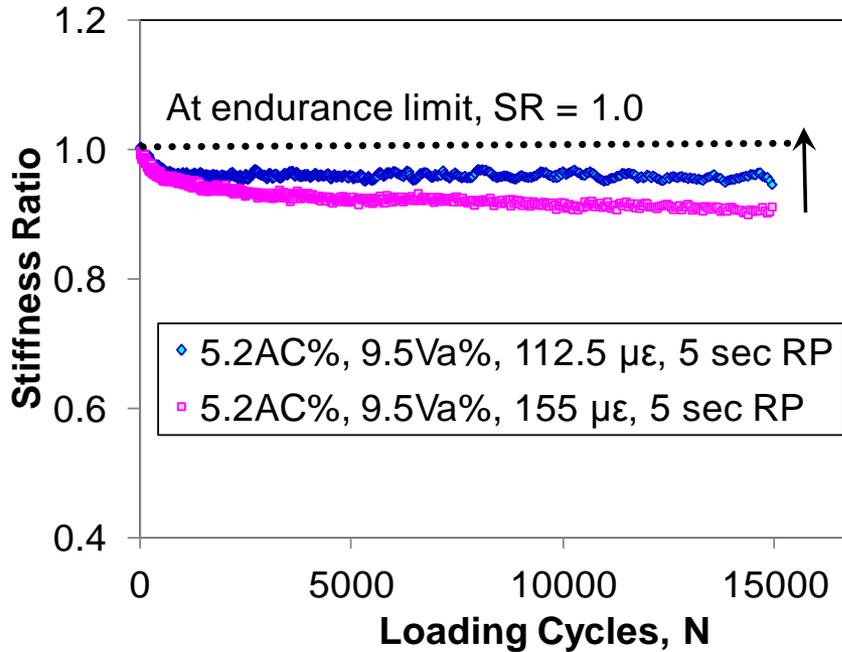


Test With Rest Periods



Algorithm Development for HMA Endurance Limit

■ Determination of Endurance Limit Using SR



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First Generation SR Model

$$SR = f(T, AC, V_a, \epsilon_t, RP, BT, \text{ and } N)$$

AC = Asphalt content, %

V_a = Air voids, %

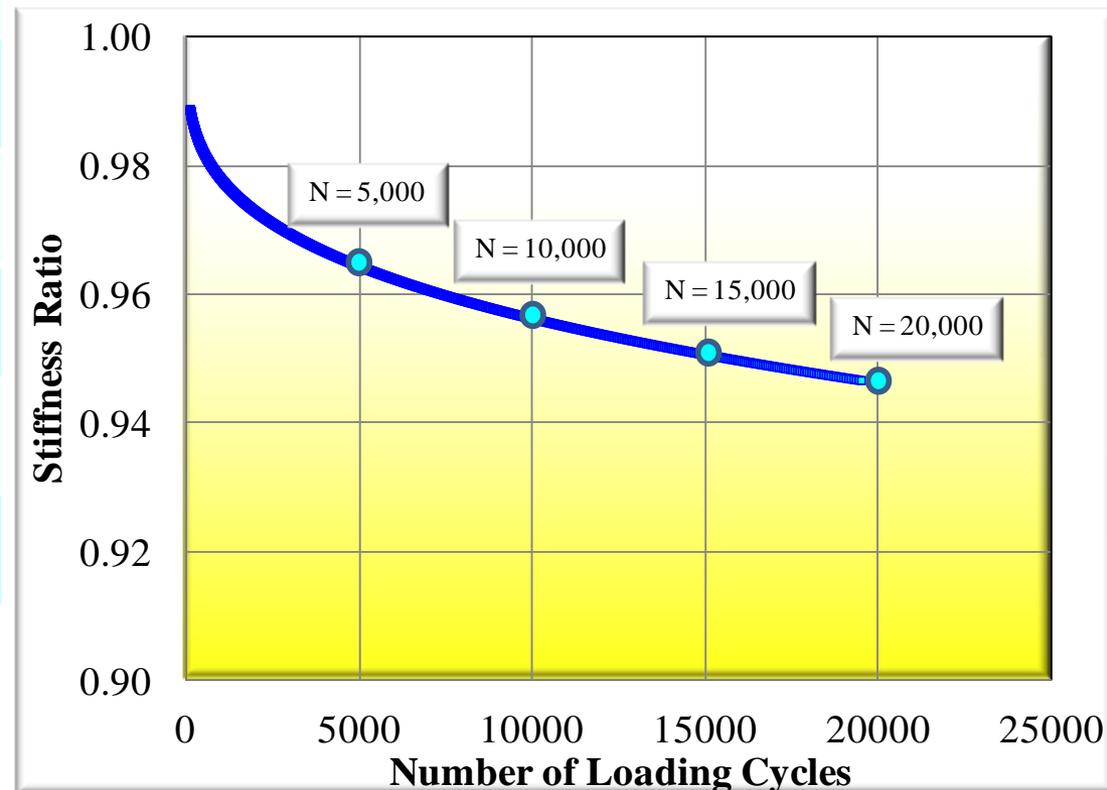
ϵ_t = Tensile Strain, μs

T = Temperature, $^{\circ}F$

RP = Rest period, sec

BT = Binder Type

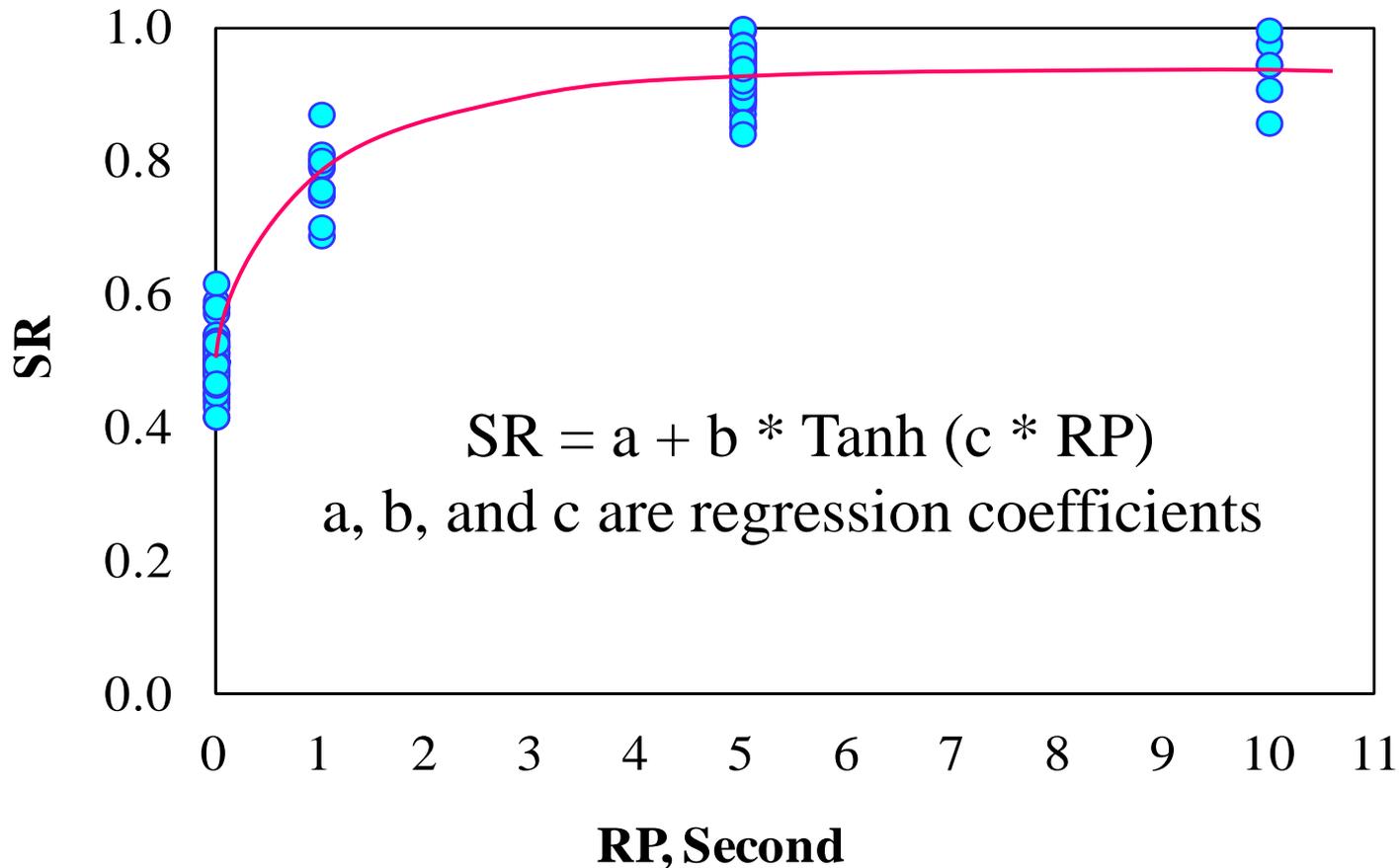
N = Number of cycles



First Generation SR Model

■ Form of First Generation SR Model

Effect of Rest Period

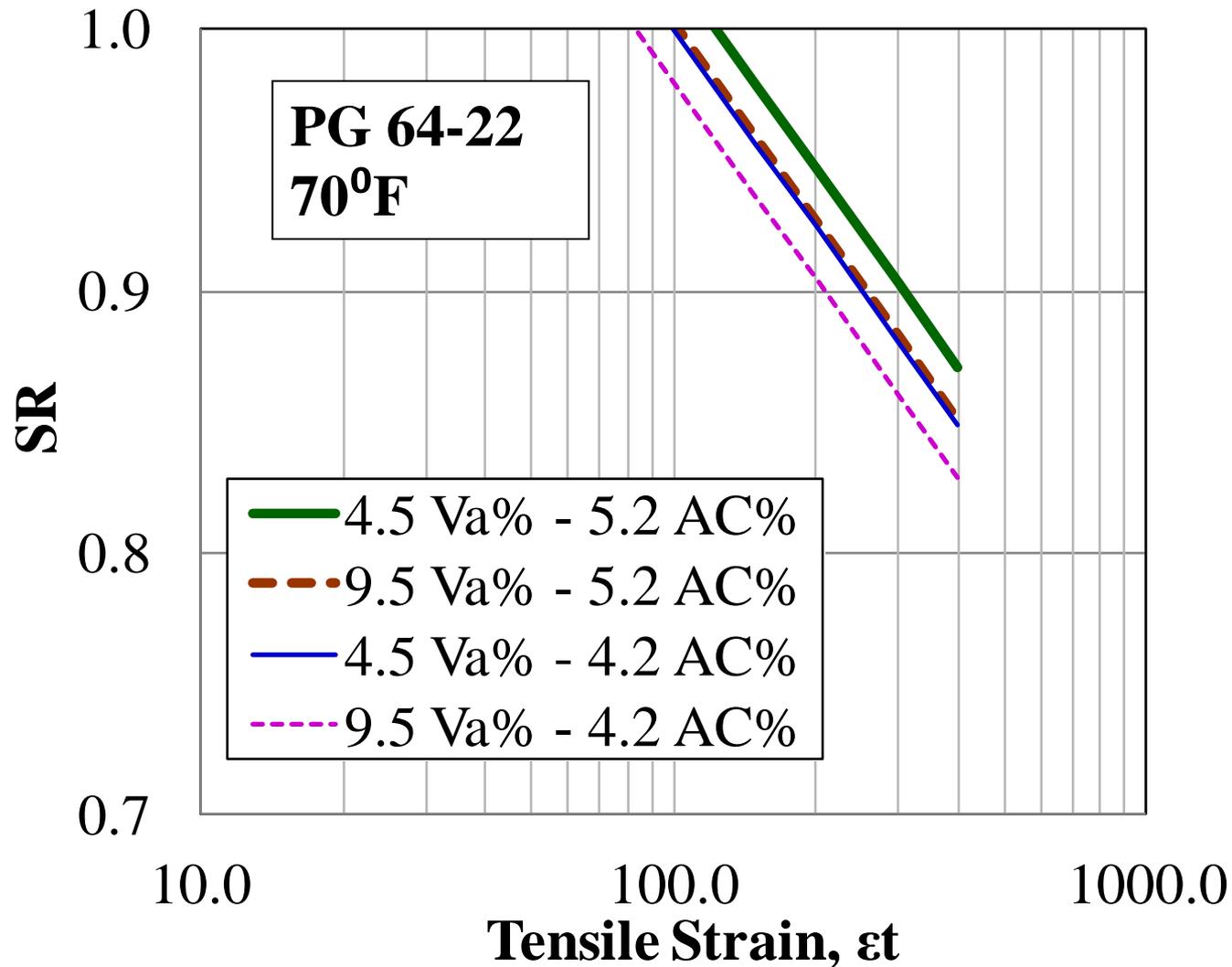


First Generation SR Model

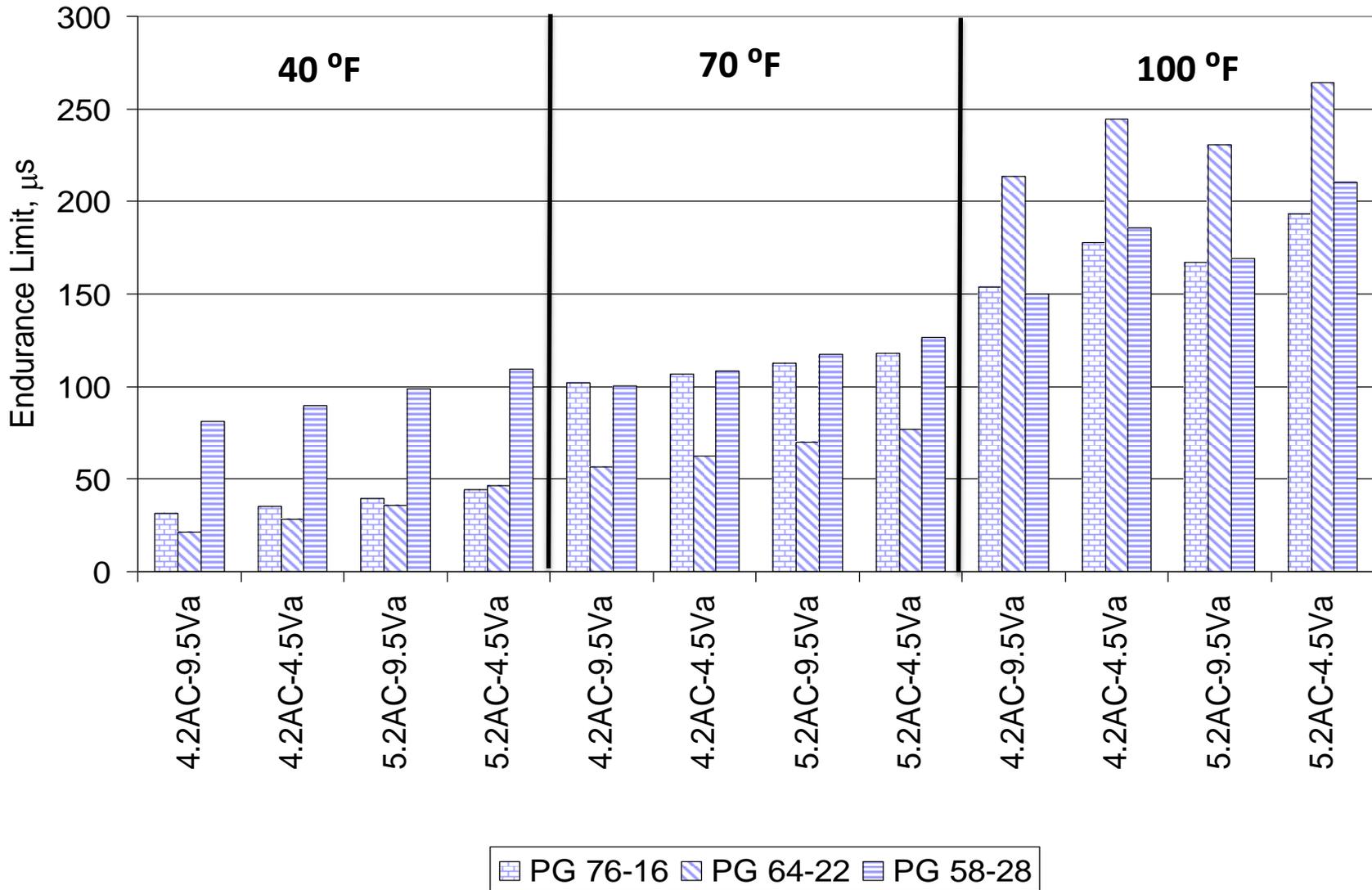
■ $R^2_{adj} = 0.979$

$$\begin{aligned}
 SR = & 0.1564774 + (0.00079*BT) + (0.070059744*AC) + \\
 & (0.00393*V_a) + (0.10095*RP) - (1.268*10^{-7} *N_f) - (0.0024676 *T) \\
 & - (0.0001677*BT*AC) + (3.29961x10^{-5} *BT*RP) + (3.488*10^{-6} \\
 & *BT*T) + (0.00794848*AC*RP) - (0.0042225*V_a*RP) + \\
 & (0.0006044*AC*T) - (0.0001035*V_a*T) - (2.889*10^{-8}*RP*N_f) + \\
 & (2.9191*10^{-9} *N_f*T) - (0.0025*RP*T) - (3.97*10^{-7} *BT^2) - \\
 & (1.20135*10^{-5}*T^2) + (8.434*10^{-8} *BT^2*AC) - (2.8756*10^{-8} \\
 & *BT^2*RP) + (1.9558*10^{-6} *AC*T^2) + (6.6137*10^{-7} *V_a*T^2) - \\
 & (1.582*10^{-11} *N_f*T^2) + (1.262x10^{-5} *RP*T^2) - (1.176*10^{-6} \\
 & *V_a*RP*T^2) + (3.124*10^{-12} *N_f*RP*T^2) - (7.4*10^{-7} *BT*AC*T) \\
 & + (3.92*10^{-7} *BT*RP*T) + (0.00013185 *V_a*RP*T) + (2.19 * 10^{-9} \\
 & *N_f*RP*T)
 \end{aligned}$$

EL Values From First Generation SR Model



EL Values From First Generation SR Model



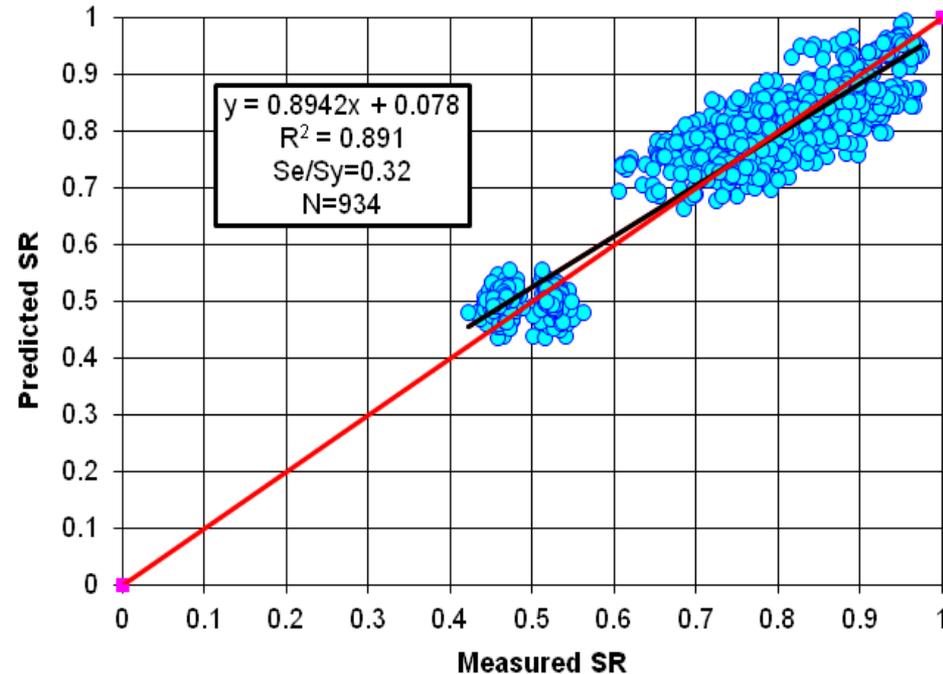
Second Generation PSR Model

- BT, T, AC, V_a were replaced by initial stiffness, E_o

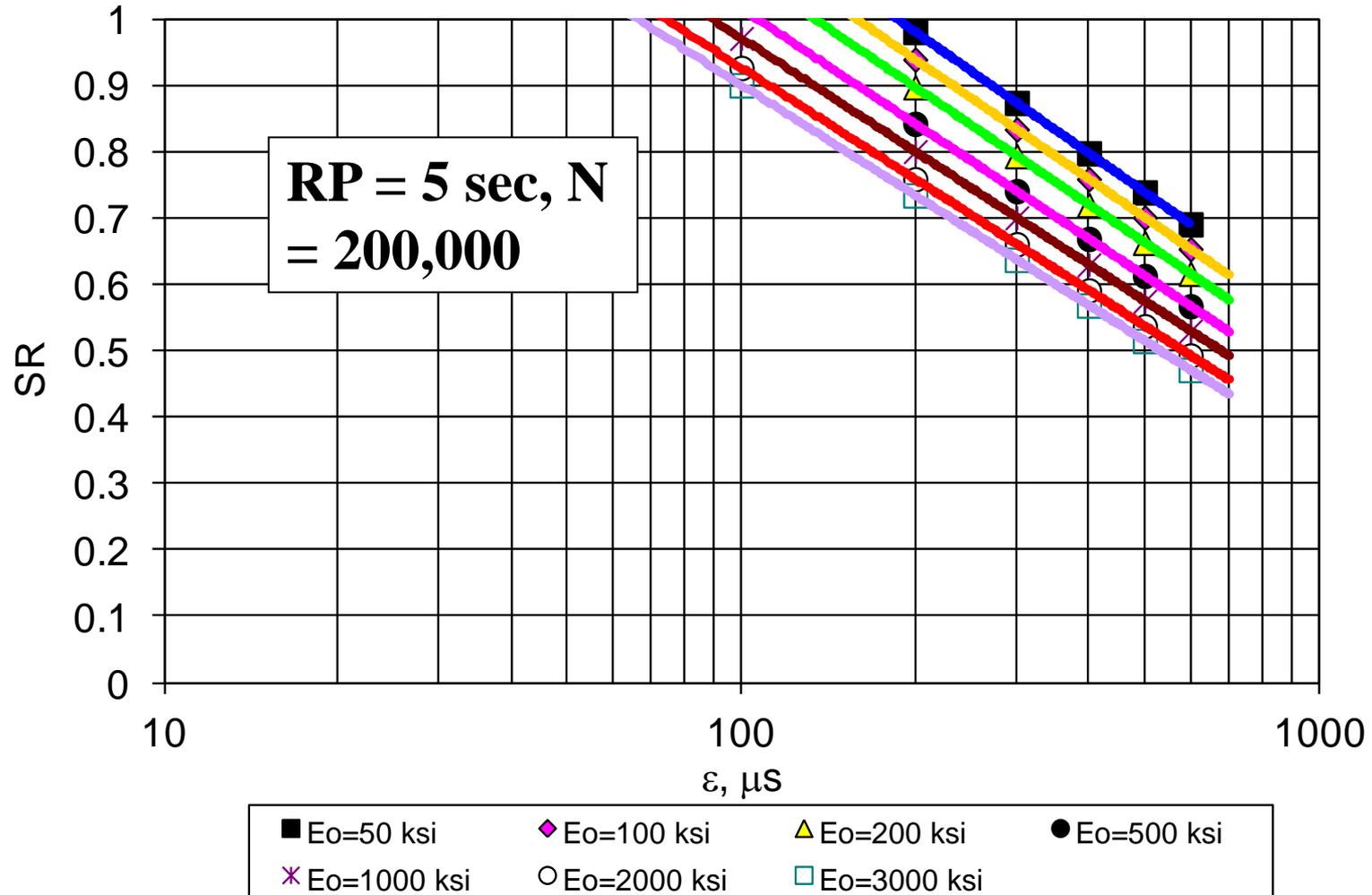
$$SR = f(E_o, \varepsilon_t, RP, \text{ and } N)$$

- $R^2_{adj} = 0.891$

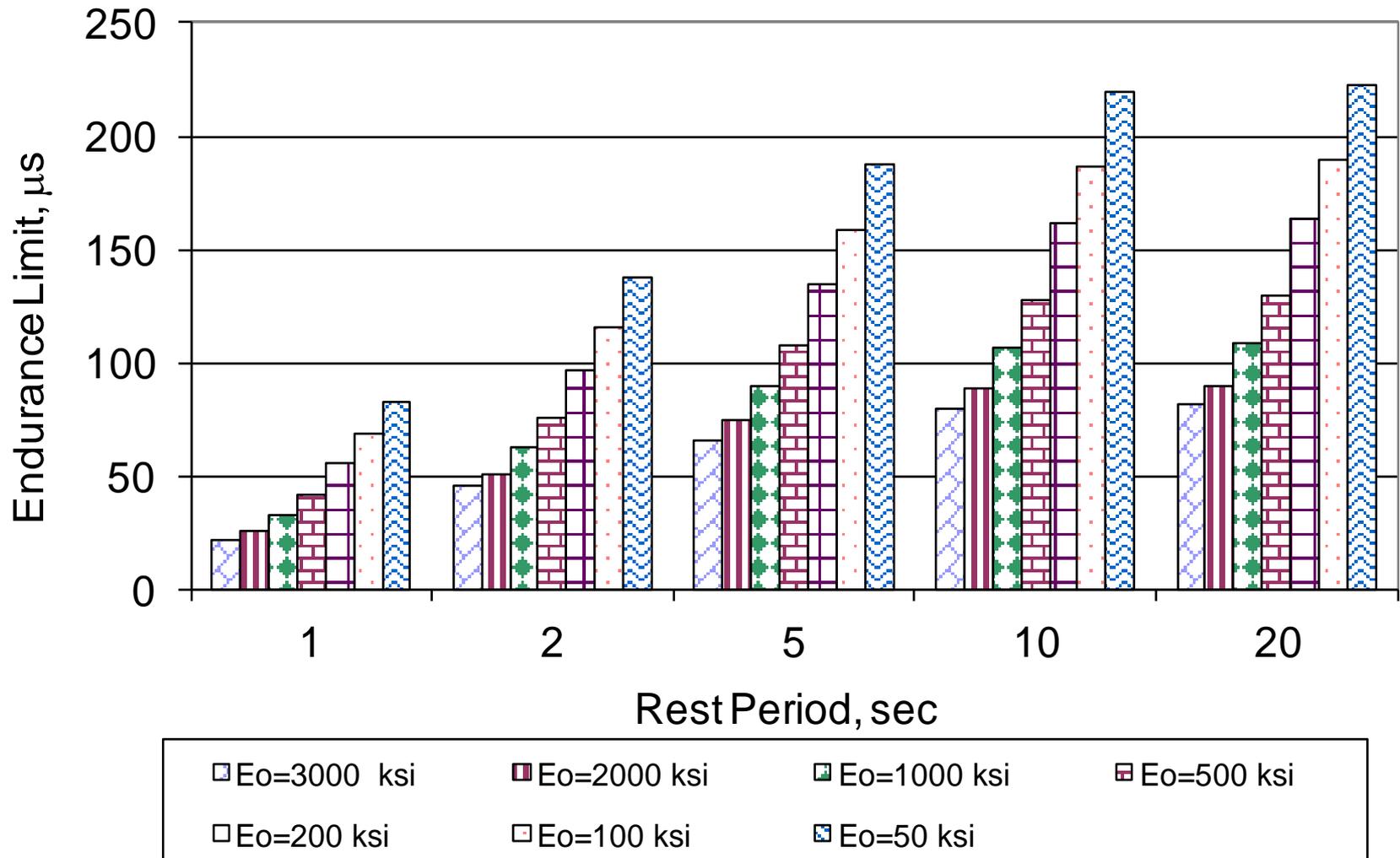
$$\begin{aligned} SR = & 2.0844 - 0.1386 * \log(E_o) - \\ & 0.4846 * \log(\varepsilon_t) - 0.2012 * \log(N) + \\ & 1.4103 * \tanh(0.8471 * RP) + 0.0320 \\ & * \log(E_o) * \log(\varepsilon_t) - 0.0954 * \log(E_o) \\ & * \tanh(0.7154 * RP) - \\ & 0.4746 * \log(\varepsilon_t) * \tanh(0.6574 * RP) \\ & + 0.0041 * \log(N) \\ & * \log(E_o) + 0.0557 * \log(N) * \log(\varepsilon_t) + \\ & 0.0689 * \log(N) * \tanh(0.0259 * RP) \end{aligned}$$



Second Generation SR Model



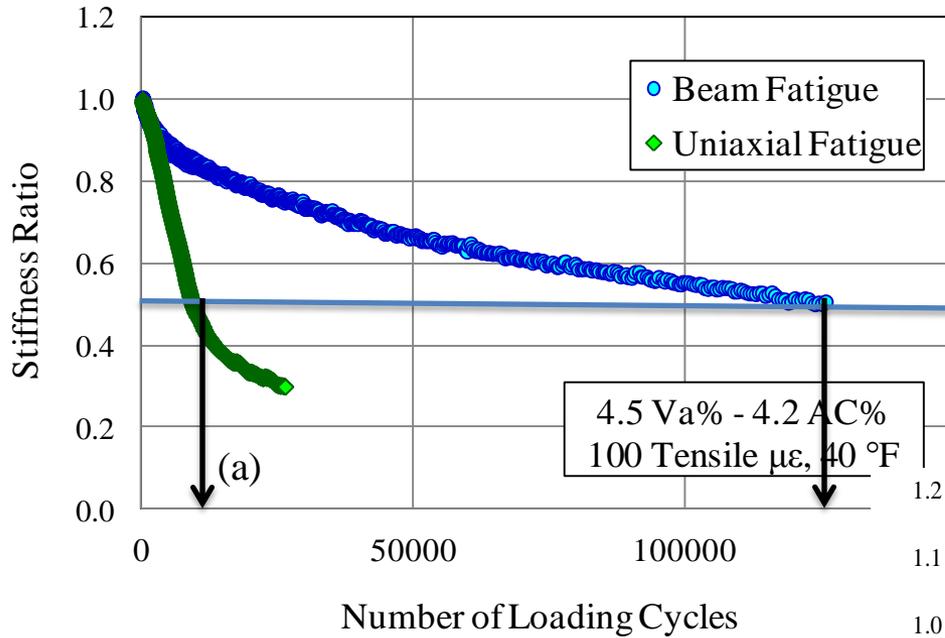
EL from Second Generation SR Model



Outline

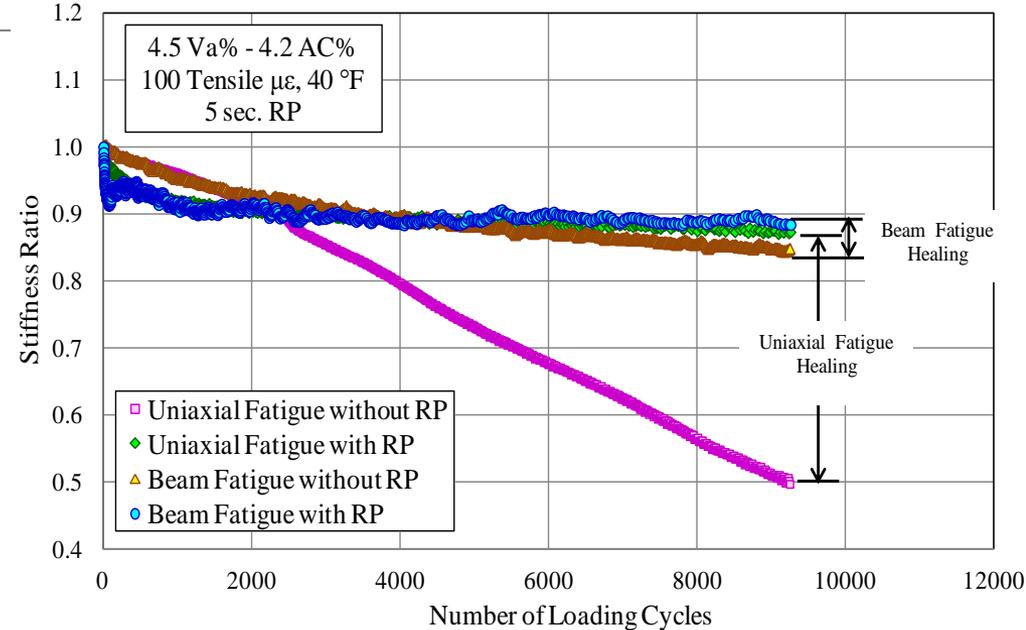
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Beam Fatigue Versus Uniaxial Fatigue Tests

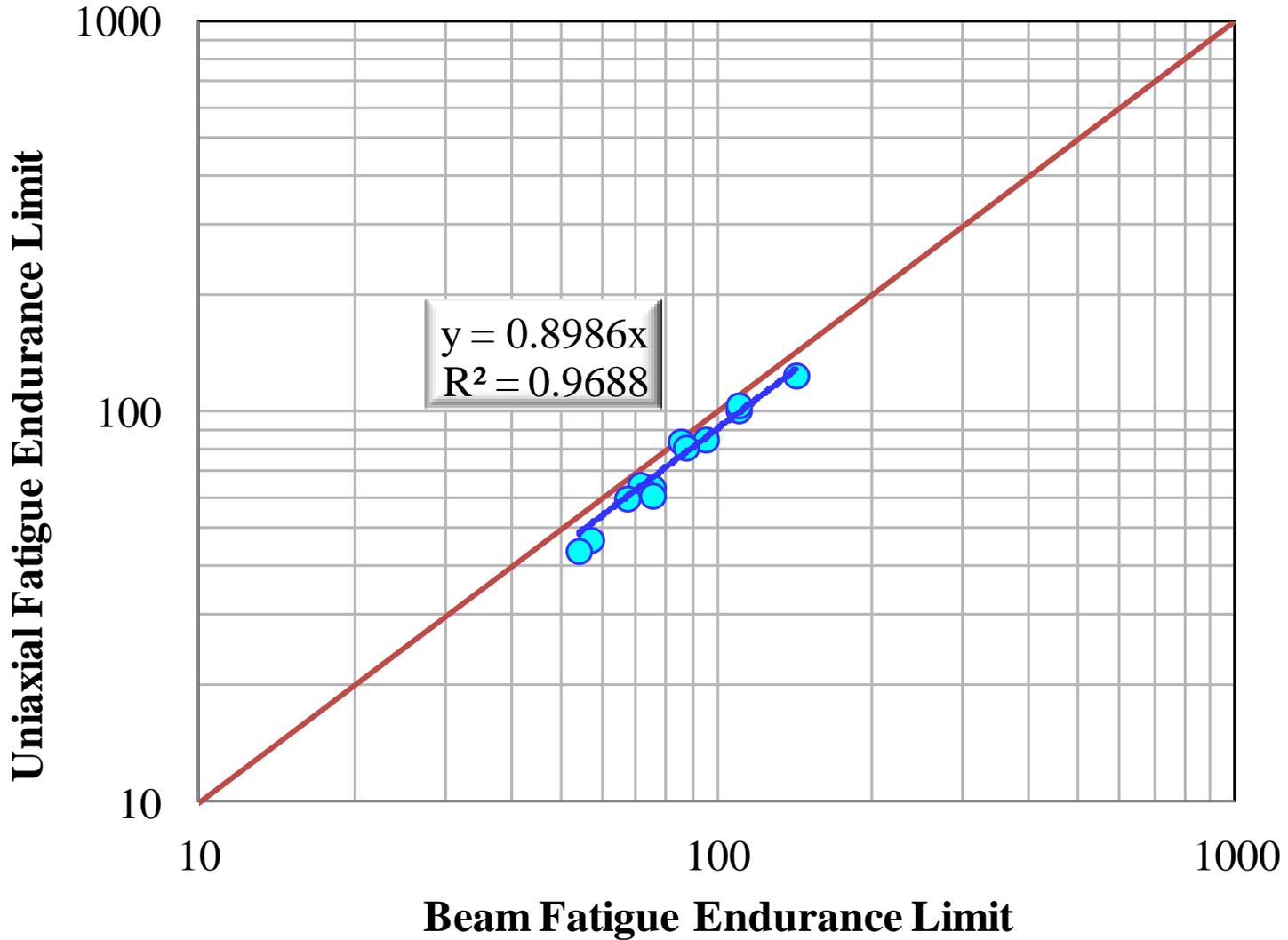


Damage Comparison

Healing Comparison



Uniaxial Fatigue Versus Beam Fatigue



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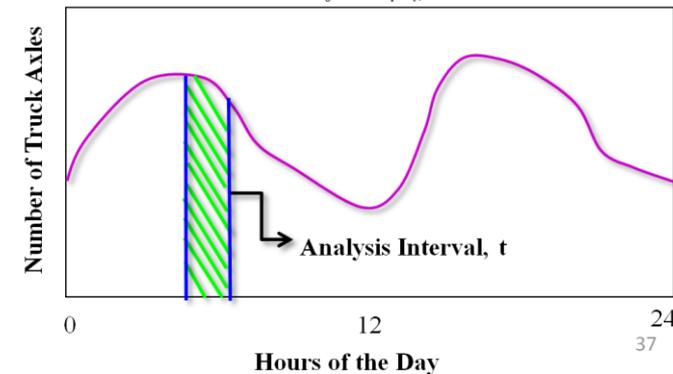
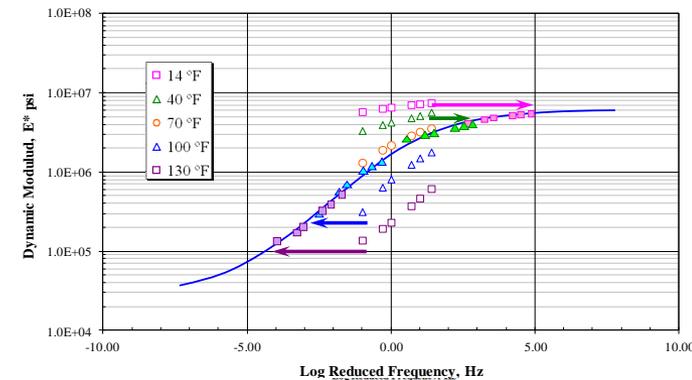
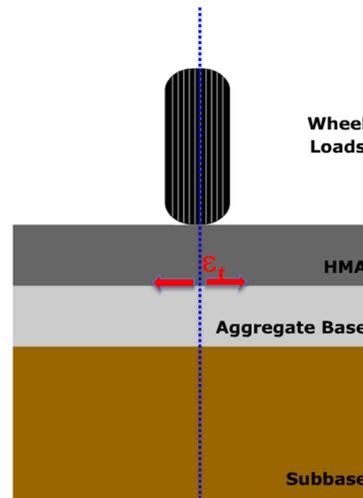
Incorporation of EL into AASHTOWare-ME

1. Calculation of Endurance Limit

$$SR = f(E_o, \epsilon_t, N, \text{ and } RP)$$

- E_o , Initial Stiffness (ksi)
- N = Number of cycles
 N of 20,000 is recommended
- RP = Rest Period (sec)
 $RP = t / \sum(NT)$

- ϵ_t , Tensile Strain, μs
 Tensile Strain is equal to the
 Endurance Limit at $PSR = 1.0$



Incorporation of EL into AASHTOWare-ME

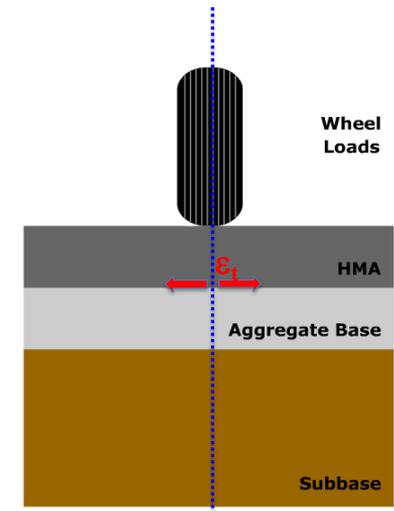
2. Incorporation of EL into Fatigue Damage

$$D_i = \sum (n_i / N_{f_i})$$

D = Fatigue Damage

n_i = Actual traffic for period i (Traffic Demand)

N_{f_i} = Allowed Traffic in period i (Traffic Capacity)



If the calculated EL $<$ the actual ϵ_t , Damage is count

If the calculated EL \geq the actual ϵ_t , the N_i is infinity and the Damage is zero

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Conclusions

- HMA exhibits endurance limit
- Mixtures using softer binders exhibit higher endurance limits than mixtures using stiffer binders
- High binder contents and low air voids produced the high endurance limit values
- Endurance limit values were higher at high temperatures
- The endurance limit values from the beam fatigue exhibit similar trends compared to those of the uniaxial fatigue test
- The endurance limits obtained in this study can be incorporated in the AASHTOWare-ME

Recommendations

- Field calibration is needed
- Consider other types of aggregates, and mixes such as warm mix asphalt, asphalt rubber, and polymer modified mixtures

Acknowledgement

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Questions!

