



U.S. Department  
of Transportation  
Federal Highway  
Administration



# GEOSYNTHETIC REINFORCED SOIL INTEGRATED BRIDGE SYSTEM

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# EDC

- Taking effective, proven and market-ready technologies and getting them into widespread use

[www.fhwa.dot.gov/everydaycounts](http://www.fhwa.dot.gov/everydaycounts)

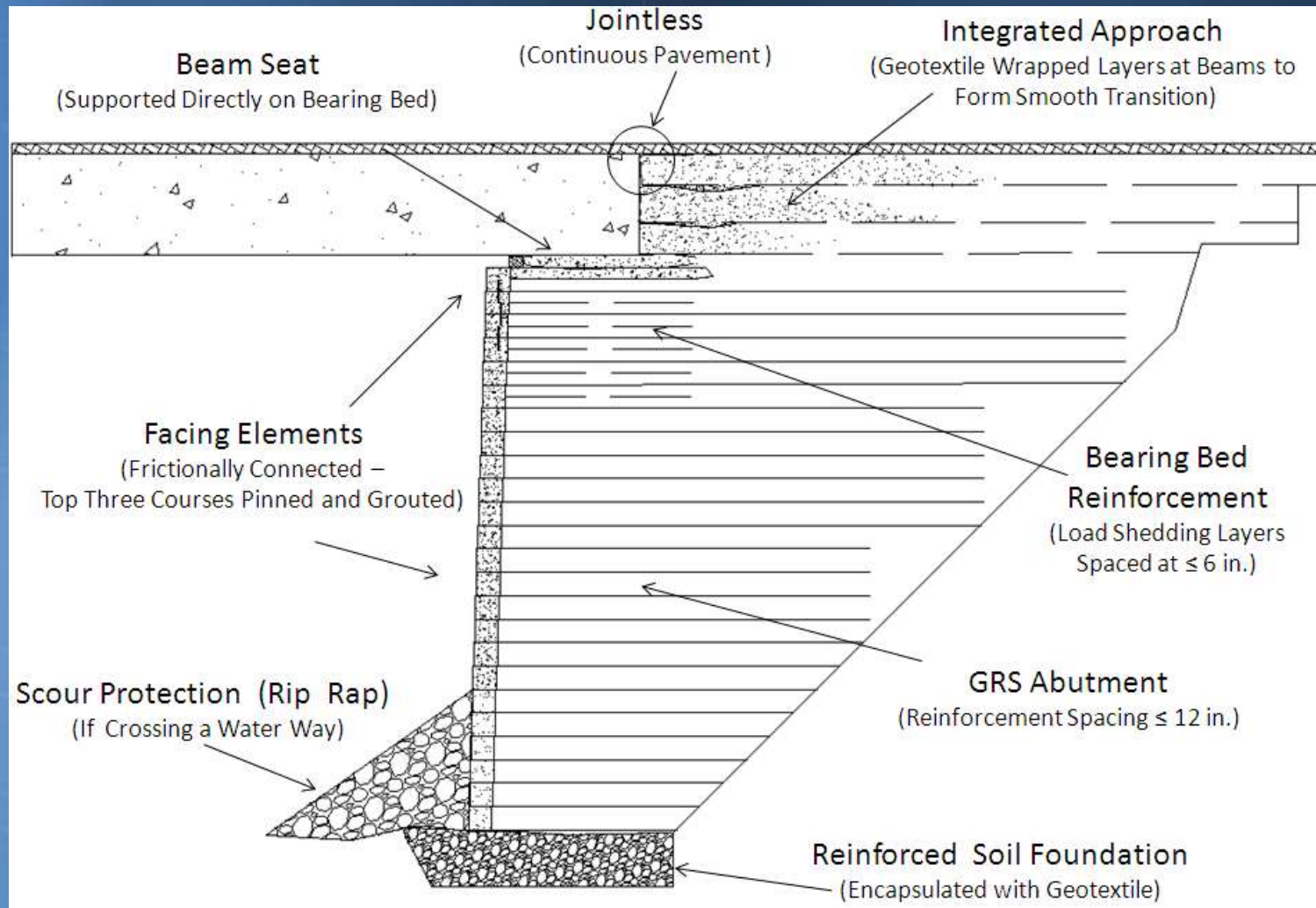


# Definitions

- **GRS - Geosynthetic Reinforced Soil**
  - An engineered fill of closely spaced ( $< 12''$ ) alternating layers of compacted granular fill material and geosynthetic reinforcement
- **IBS - Integrated Bridge System**
  - A fast, cost-effective method of bridge support that blends the roadway into the superstructure using GRS technology



# Cross-Section of GRS-IBS





# Summary of Benefits

- Reduced construction cost (25 - 60%)
- Reduced construction time
- Construction less dependent on weather conditions
- Flexible design - easily field modified for unforeseen site conditions (e.g. obstructions, utilities, different site conditions)
- Easier to maintain (fewer bridge parts)
- QA/QC Advantages





# Site Selection

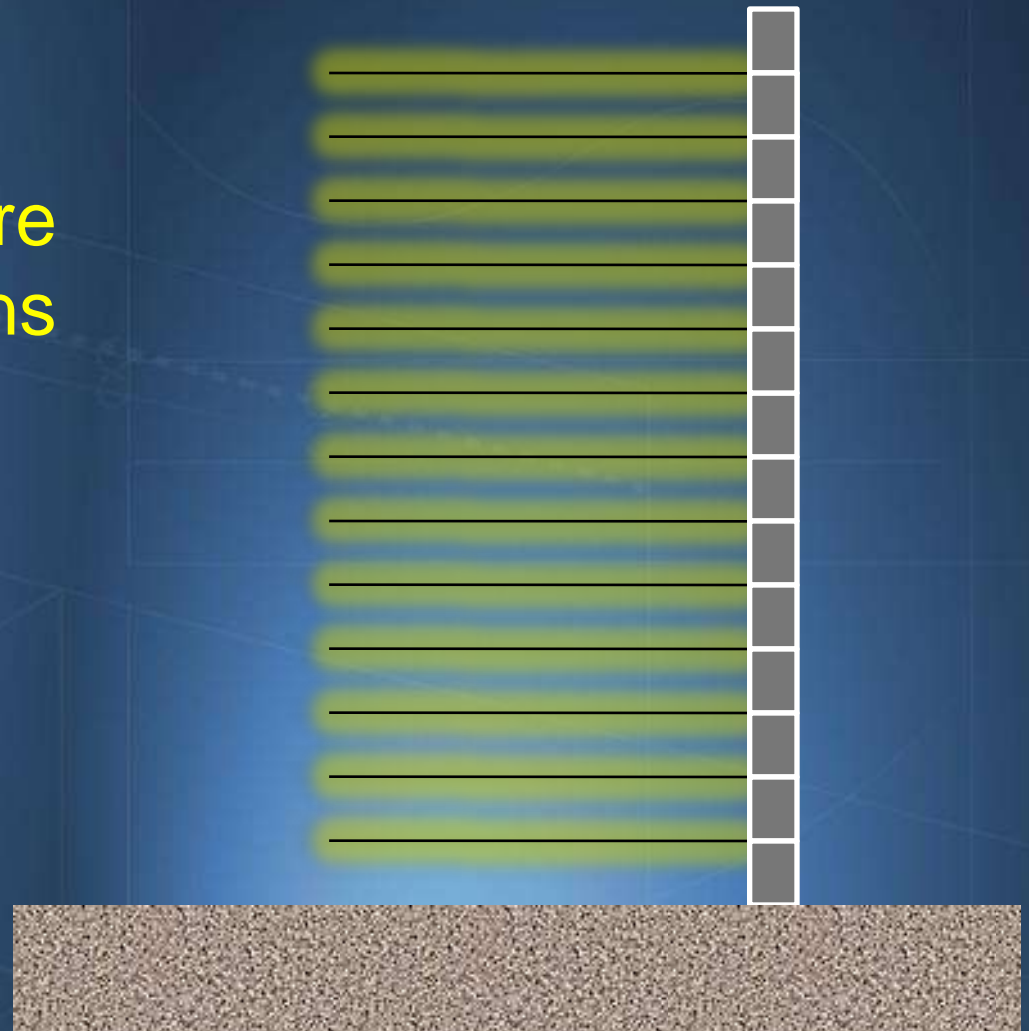
- Single span (currently 140 ft)
- 30 ft abutment height
- Grade separation
- Water crossings with low scour potential
- Steel or concrete superstructures
- New or replacement structures



# Composite Behavior

## GRS

- Composite Structure
- Friction Connections
- Close Spacing





# Performance Tests

Before



After







# Performance Test

## 2400 lb/ft @ 8" Spacing

Before



After





0.5 ksf  
(25 kPa)





4.1 ksf  
(196 kPa)





6.8 ksf  
(326 kPa)





10.3 ksf  
(493 kPa)





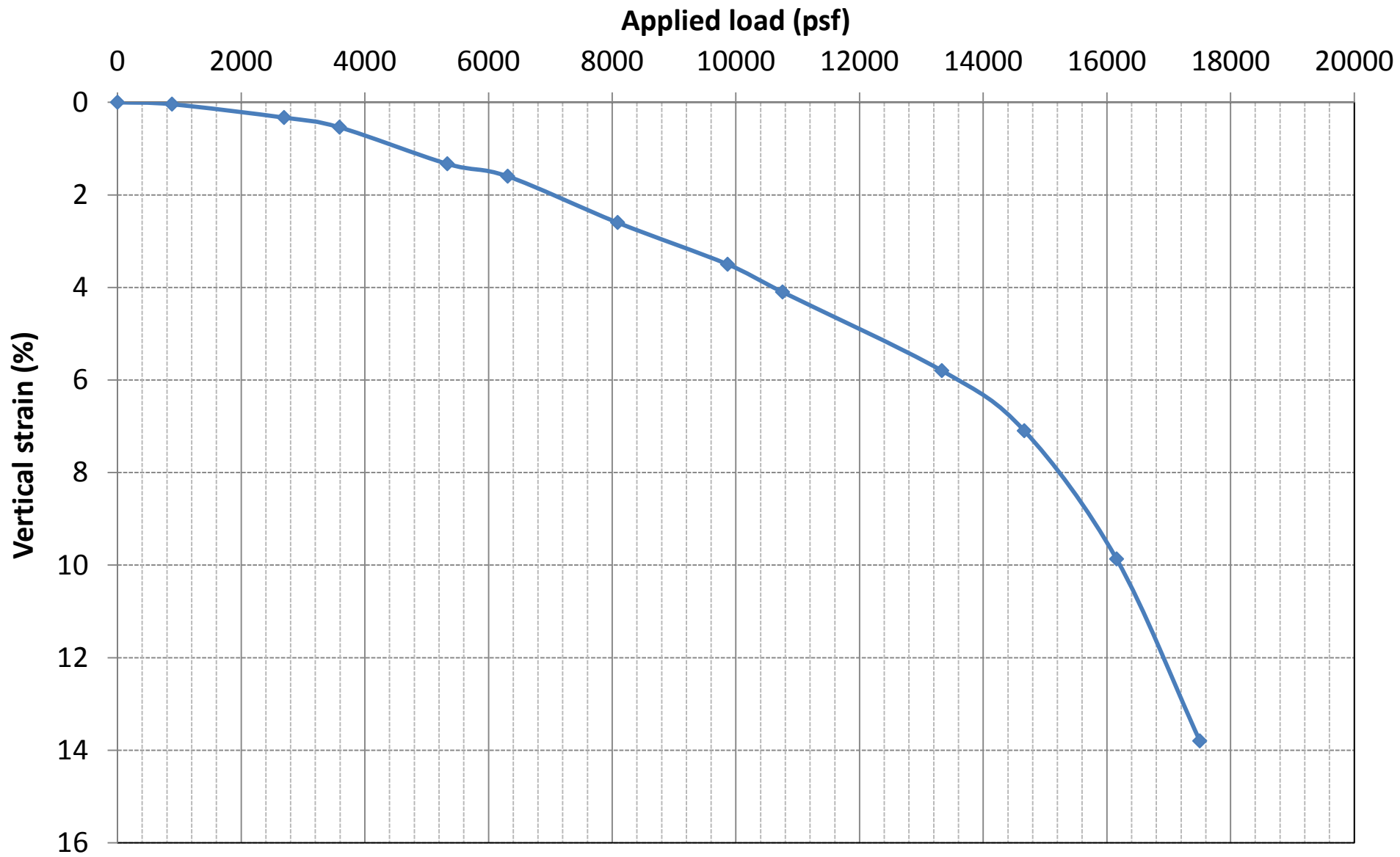
13.9 ksf  
(666 kPa)





18.1 ksf  
(867 kPa)

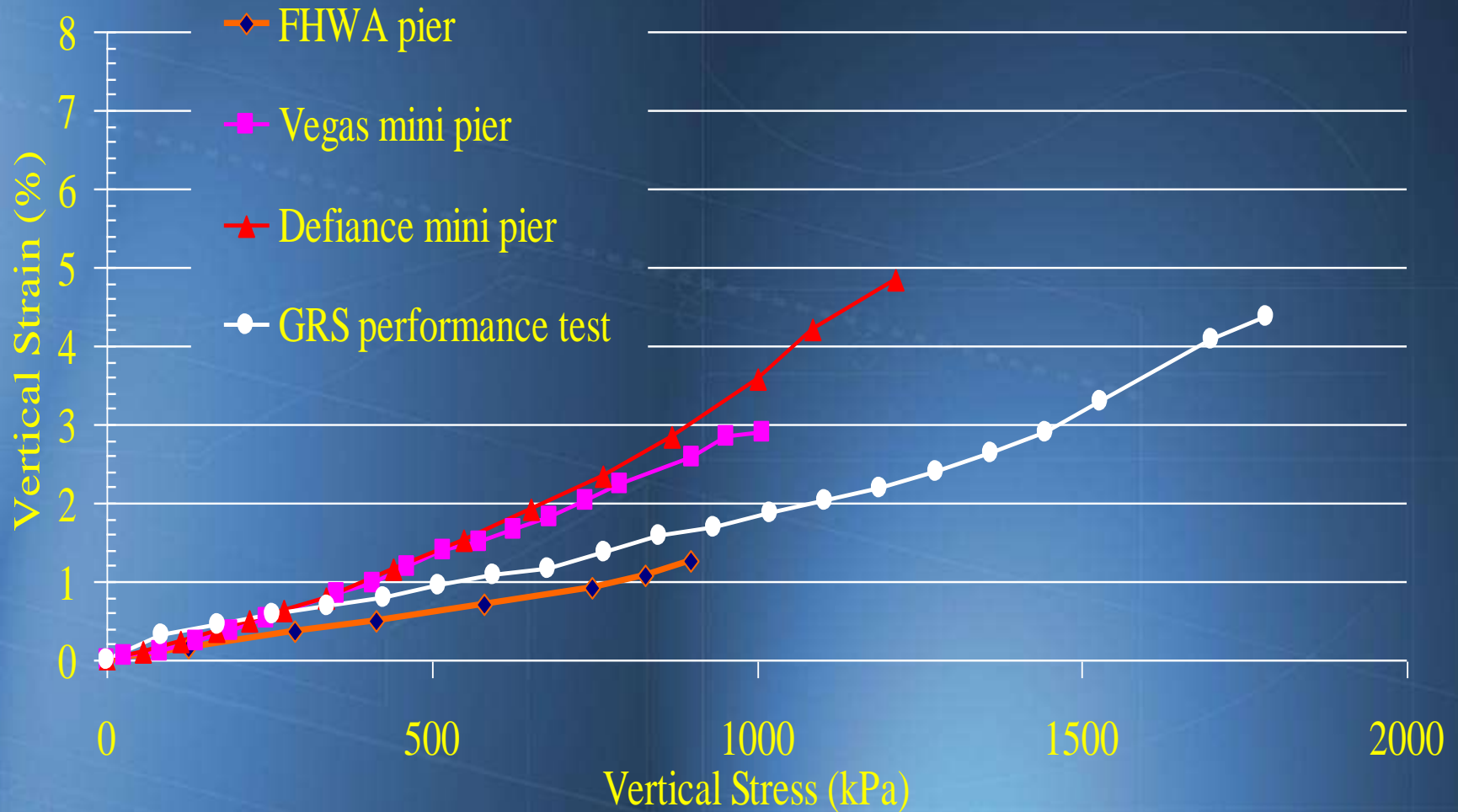






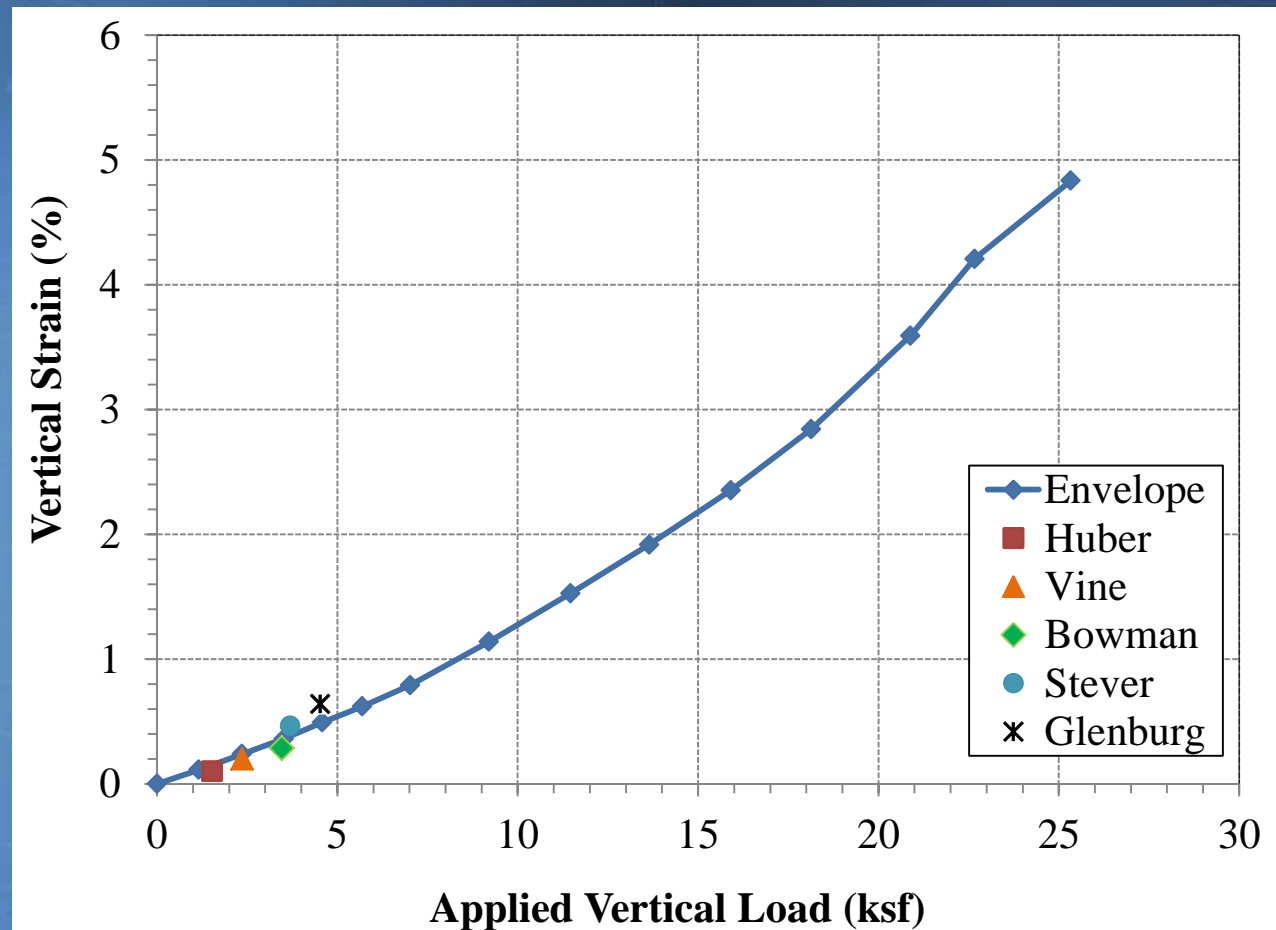


# Performance Test Results





# Vertical Deformation *Continued*





# GRS IBS Reports

## Geosynthetic Reinforced Soil Integrated Bridge System Interim Implementation Guide

PUBLICATION NO. FHWA-HRT-11-026

JANUARY 2011



U.S. Department of Transportation  
Federal Highway Administration

Research, Development, and Technology  
Turner-Fairbank Highway Research Center  
6300 Georgetown Pike  
McLean, VA 22101-2296

## Geosynthetic Reinforced Soil Integrated Bridge System Synthesis Report

PUBLICATION NO. FHWA-HRT-11-027

JANUARY 2011



U.S. Department of Transportation  
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Research, Development, and Technology  
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STATE	PROJECT	SHEET NUMBER
	FHWA DGS-IBS	A



## INDEX TO SHEETS

- A. COVER SHEET AND NOTES
- B. QUANTITIES & DESIGN DIMENSIONS
- C. PLAN AND ELEVATION FACING BLOCK SCHEDULE
- D. GRS-18S ABUTMENT DETAILS

**PURPOSE:** These example plan Sheets A through D were prepared to illustrate the typical contents of a set of drawings necessary for a GR5-1BS project. Presented in these plans are the assumptions for the bridge and GR5-1BS systems with typical wall heights (H) ranging from 10 to 24 feet. Two conditions were prepared for the quantity estimate Sheet B: "poor soil conditions" and "favorable soil conditions".

**INTENDED USE:** These plans are not associated with a specific project. All dimensions and properties should be confirmed and/or revised by the Engineer of record and prior to use. Project specifications should be prepared to supplement this plan set.

#### DESIGN LOADS AND SOIL PROPERTIES

Combined load: Superstructure ( $q_{LL} + q_8$ ) 2 TSF maximum (service load, allowable stress design). Roadway live load surcharge: 250 psf uniform vertical

Road Base unit weight = 140 pcf. thickness = 34-inches

**"Poor" Soil Conditions:**  
 Retained backfill: Unit weight = 125 pcf, friction angle = 34°, cohesion = 0 pcf,  
 (Cohesion > 200 pcf assumed for temporary back slope cut conditions  
 during construction.)  
 d<sub>max</sub> > 1.0 inches  
 Reinforced fill: Unit weight = 115 pcf, friction angle = 38°, cohesion = 0 pcf  
 RSF backfill: Unit weight = 140 pcf, friction angle = 38°, cohesion = 0 pcf  
 Foundation soil: Unit weight = 125 pcf, friction angle = 30°, cohesion = 0 pcf

**\*Favorable\* Soil Conditions:**  
 Retained backfill: Unit weight = 125 pcf, friction angle = 40°, cohesion = 100 psf  
 $\phi_{max} > 0.5$ -inches  
 Foundation soil: Unit weight = 125 pcf, friction angle = 40°, cohesion = 100 psf  
 Reinforced fill: Unit weight = 120 pcf, friction angle = 42°, cohesion = 0 psf  
 RSF backfill: Unit weight = 120 pcf, friction angle = 42°, cohesion = 0 psf

## DESIGN SPECIFICATIONS

1. Geosynthetic Reinforced Soil Integrated Bridge System Interim Implementation Guide, FHWA-HRT-11-026, January 2011.
2. Design methods follow the ASD design methods presented in Chapter 4 of the reference Manual. No seismic design assumed.
3. Conduct a subsurface investigation in accordance with "Soils and Foundations", FHWA-NHI-06-088 (2006) and "Subsurface Investigations", FHWA-NHI-01-031, (2006).
4. Design factor of safety against sliding is  $\geq 1.5$ ; Factor of safety against bearing failure is  $\geq 2.5$ .
5. A global stability analysis must be performed for each site. Factor of safety against global failure is to be  $\geq 1.5$ .
6. Performance criteria: tolerable vertical strain = 0.5% of wall height (H); tolerable lateral strain = 1.0% of  $h$  and  $a$ , (bearing width and setback).

7. Settlement below the RSF is assumed to be negligible. No differential settlement between abutments is assumed.
8. Sliding checks were conducted at the top and bottom of the RSF to meet the minimum factors of safety in the reference manual.
9. Road base thickness ( $h_{rb}$ ) assumes a 32-inch structure and 2-inch pavement thickness.

### CONSTRUCTION SPECIFICATIONS

1. **Site Layout/Survey:** Construct the base of the GRS abutment and wingwalls within 1.0 inch of the staked elevations. Construct the external GRS abutment and wingwalls to within  $\pm 0.5$  inches of the surveyed stake dimensions.
2. **Excavation:** Comply with Occupational Safety and Health Administration (OSHA) for all excavations.
3. **Compaction:** Compact backfill to a minimum of 95 percent of the maximum dry density according to AASHTO T-99 and  $\pm 2$  percent optimum moisture content in the bearing reinforcement zone. Compact to 100 percent of the maximum dry density according to AASHTO T-99. Only hand-operated compaction equipment is allowed within 3-feet of the wall face. Reinforcement extends directly beneath each layer of CMU blocks, covering  $\geq 85\%$  of the full width of the block to the front face of the wall.
4. **Geosynthetic Reinforcement Placement:** Pull the geosynthetic taught to remove any wrinkles and lay flat prior to placing and compacting the backfill material. Splices should be staggered at least 24-inches apart and splices are not allowed in the bearing reinforcement zone. No equipment is allowed directly on the geosynthetic. Place a minimum 6-inch layer of granular fill prior to operating any rubber-tired equipment over the geosynthetic at speeds less than 5 miles per hour with no sudden braking or sharp turning.
5. **RSF Construction:** The RSF should be encapsulated in geotextile reinforcement on all sides with minimum overlaps of 3.0 feet to prevent water infiltration. Wrapped corners need to be tight without exposed soil. Compact backfill material in lifts less than 6-inches in compacted height. Grade and level the top of the RSF prior to final encapsulation, as this will serve as the leveling pad for the CMU blocks of the GRS abutment.
6. **GRS Wall Face Alignment:** Check for level alignment of the CMU block row at least every other layer of the GRS abutment. Correct any alignment deviations greater than 0.25 inches.
7. **Beam Seat Placement:** Generally, the thickness of the beam seat is approximately 8 to 12 inches and consists of a minimum of two 4-inch lifts of wrapped face GRS. Place precut 4-inch thick foam board on the top of the bearing bed reinforcement butt against the back face of the CMU block. Set half-height or full height (depending on wall height and required clear space) solid CMU blocks on top of the foam board. Wrap two approximately 4-inch lifts across the beam seat. Before joining the final wrap, it may be necessary to grade the surface aggregate of the beam seat slightly high, to about 0.5 inches, to aid in seating the superstructure and to maximize contact with the bearing area.

8. **Superstructure Placement:** The crane used for the placement of the superstructure can be positioned on the GRS abutment provided the outrigger pads are sized for less than 4,000 psf near the face of the abutment wall. Greater loads could be supported with increasing distance from the abutment face if checked by the Engineer of Record. An additional layout of geosynthetic reinforcement can be placed between the beam seat and the concrete or steel beams to provide additional protection of the beam seat. Set beams square and level without dragging across the beam seat surface.
9. **Integrated Approach Placement:** Following the placement of the superstructure, geotextile reinforcement layers are placed along the back of the superstructure, with a maximum lift height of 6-inches (measured vertical spacing of reinforcement  $\leq$  6-inches). The top of the final wrap should be approximately 2-inches below the top of the superstructure to allow at least 2-inches of aggregate base cover over the geosynthetic to protect it from hot mix asphalt.

### REINFORCING STEEL

Provide reinforcing steel conforming to ASTM A615, GR. 60

## CMU BLOCK

In colder climates, freeze-thaw test (ASTM C1262-10) should be concluded to assess the durability of the CMU and ensure it follows the standard specification (ASTM C1372). Additives can be used to reduce efflorescence at the face of the blocks if they are at locations subject to de-icing chemicals.

Compressive strength = 4,000 psi minimum

Water absorption limit = 5 %

$M_{\text{stock}} = 7\%$      $L_{\text{stock}} = 15\%$      $b_{\text{stock}} = 7\%$

Note: In many construction applications CMU blocks are placed with a  $\frac{3}{8}$ " mortar joint to create an in place nominal dimension of 8" x 8" x 16".

## REINFORCED BACKFILL GRADATION

**Reinforced Backfill Gradation** – See Geosynthetic Reinforced Soil Integrated Bridge System Interim Implementation Guide, Table 1 or Table 2. Consider GRS CMU minimal dimensions to be the same.

#### GEOSYNTHETIC REINFORCEMENT TENSILE PROPERTIES

Required ultimate tensile strength = 4,800 lb/ft by (ASTM D 4595 (geotextiles) or ASTM D 6637 (geogrids))  
Tensile strength at 2% strain = 1,370 lb/ft

POLYSTYRENE FOAM BOARD

Provide polystyrene foam board conforming to AASHTO M230, type VI.

U.S. DEPARTMENT OF TRANSPORTATION  
FEDERAL HIGHWAY ADMINISTRATION  
WESTERN FEDERAL LANDS-HIGHWAY DIVISION

GRS-IBS  
COVER SHEET

NO.		DATE	BY	REVISIONS	NO.		DATE	BY	REVISIONS	DESIGNED BY	DRAWN BY	CHECKED BY	SCALE	PROJECT TEAM LEADER	BRIDGE DRAWING	DATE	DRAWING NO.
	03/25/11			Rev. 0		04/04/11			Rev. 1	THWA	C. TUTTLE	R. BARROWS, B. COLLINS, M. DOORON, K. ELIAS A. ALZAMORA, J. NICKS	NTS	M. ADAMS	1 of 4	04/2011	



GRS-JBS Poor Soil Condition Quantities Per Abutment

HEIGHT (H) (FT)	ROAD BASE H & THICKNESS (IN)	GEOSYNTHETIC REINFORCEMENT (SOYD)	CMU BLOCK HOLLOW (EA)	CMU BLOCK SOLID (EAC H)	# REBAR (FT)	GRS BACKFILL (CUYD)	RSF FILL (CUYD)	FOAM BOARD (SQFT)	ROAD BASE AGGREGATE (CUYD)	CONCRETE BLOCK WALL FILL (CUYD)
10.42	34	1200	730	349	652	287	52	18	54	1.4
12.32	34	1700	950	365	688	399	73	18	63	1.5
14.31	34	2100	1165	373	721	509	94	18	68	1.6
16.22	34	2700	1455	389	766	655	123	18	77	1.7
18.21	34	3200	1700	397	789	793	154	36	82	1.7
20.12	34	4000	2030	413	833	973	187	36	92	1.8
22.1	34	4600	2305	421	858	1139	220	36	96	1.9
24.07	34	5600	3280	437	904	1354	267	36	106	2

GRS-IBS ABUTMENT Favorable Soil Condition Quantities Per Abutment<sup>1</sup>

HEIGHT (H) (FEET)	ROAD BASE H <sub>10</sub> THICKNESS (IN)	GEOSYNTHETIC REINFORCEMENT (SQYD)	CMU BLOCK HOLLOW (EACH)	CMU BLOCK SOLID (EACH)	RE REBAR (FEET)	GRS BACKFILL (CUYD)	RSF FILL (CUYD)	FOAM BOARD (SQFT)	ROAD BASE AGGREGATE (CUYD)	CONCRETE BLOCK WALL FILL (CUYD)
10.42	34	1000	710	349	652	176	24	18	54	1.4
12.32	34	1400	950	363	698	242	26	18	63	1.5
14.31	34	1700	1165	373	721	305	27	18	68	1.6
16.22	34	2200	1455	389	766	394	29	18	77	1.7
18.21	34	2700	1700	397	789	483	35	36	82	1.7
20.12	34	3400	2030	413	835	606	43	36	92	1.8
22.1	34	4000	2305	421	858	715	50	36	96	1.9
24.01	34	4800	2880	437	904	865	60	36	108	2

**GRS-IBS Poor Soil Condition DESIGN DIMENSIONS**

WALL HEIGHT (ft)	WINGWALL LENGTH, L <sub>WW</sub>	$\frac{Z}{b}$	$\alpha_0$	b	b <sub>1</sub>	$\delta_{total}$	$\delta$	$\delta_{RSP}$	D <sub>RSP</sub>	K <sub>RSP</sub>	ABUT WIDTH	WINGWALL HEIGHT
(FT)	(FT)	(IN)	(IN)	(FT)	(FT)	(FT)	(FT)	(FT)	(FT)	(FT)	(FT)	(FT)
10.42	15.83	3	7.6	2.5	3.83	9.5	8.86	11.88	2.38	2.38	37.76	14.00
12.32	18.23	3	7.6	2.5	3.83	11.0	10.38	13.75	2.75	2.75	37.76	15.89
14.31	19.53	4	7.6	2.5	3.83	12.5	11.86	15.63	3.13	3.13	37.76	17.79
16.22	22.14	4	7.6	2.5	3.83	14.0	13.36	17.50	3.50	3.50	37.76	19.70
18.21	23.44	5	7.6	2.5	3.83	15.5	14.88	19.39	4.00	3.89	37.76	21.60
20.11	26.04	5	7.6	2.5	3.83	17.0	16.36	21.25	4.25	4.25	37.76	23.51
22.10	27.34	6	7.6	2.5	3.83	18.5	17.86	23.13	4.63	4.63	37.76	25.42
24.01	29.95	6	7.6	2.5	3.83	20.0	19.38	25.00	5.00	5.00	37.76	27.33

GRS/BS Favorable Soil Condition DESIGN DIMENSIONS

WALL HEIGHT (ft)	WINGWALL LENGTH, $L_{ww}$	$\theta_a$	$\theta_c$	$b$	$\theta_r$	$S_{RWR}$	$S$	$S_{RSP}$	$D_{RSP}$	$V_{RSP}$	ABUT WIDTH	WINGWALL HEIGHT
(ft)	(ft)	(in)	(in)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)
10.42	15.63	3	7.6	2.5	3.83	6.0	5.36	7.50	1.50	1.50	37.76	14.00
12.32	16.23	3	7.6	2.5	3.83	6.0	5.36	7.50	1.50	1.50	37.76	15.89
14.31	19.53	4	7.6	2.5	3.83	6.0	5.36	7.50	1.50	1.50	37.76	17.79
16.22	22.14	4	7.6	2.5	3.83	6.0	5.36	7.50	1.50	1.50	37.76	19.70
18.21	23.44	5	7.6	2.5	3.83	6.5	5.86	8.13	1.63	1.63	37.76	21.60
20.11	26.04	5	7.6	2.5	3.83	7.0	6.36	8.78	1.75	1.75	37.76	23.51
22.10	27.34	6	7.6	2.5	3.83	7.5	6.86	9.38	1.88	1.88	37.76	25.42
24.01	29.95	6	7.6	2.5	3.83	8.0	7.36	10.00	2.00	2.00	37.76	27.33

FOOTNOTES:

*J* The estimated materials quantities correspond to the dimensions on the accompanying plan sheets. Deviation from the dimensions on the plan sheets will void the quantities.

<sup>a</sup> Foam board thickness is 4-inches (typ.)

$$3) \text{ Wingwall length} = B \text{ total} + H + 3\text{-feet}$$

CMU block assumptions: solid blocks at the base of the GRS abutment, from estimated scour elevation to 100-year flood event elevation (5'-feet assumed here); solid blocks in setback location to beam seat (1'-row assumed); hollow blocks for remaining wall height and guardrail wall. Hollow blocks in row 1 of the wall are to be rough trowel parged and at the top of the wall of guardwall and at all corners: wet cast coping at the top row of exposed CMU at abutment wall and wingwall; flush concrete fill in the CMU's at the top of the abutment wall under the beam seat below the clear zone. See Sheet C and D for illustrations.

5/ Maximum vertical spacing of reinforcement = height of 1 CMU block ( $H_{block}$ ) in reinforced backfill zone. Maximum vertical spacing of reinforcement  $\leq$  6-inches in bearing bed zone and integrated approach.

*§/ No overlaps in geosynthetics measured for quantities.*

<sup>2</sup>/ Design clear space (d<sub>1</sub>) rounded up to the nearest 1.0 inch.<sup>B</sup> Geosynthetic reinforcement quantity includes RSF and IBS geotextile quantities

#### ABBREVIATIONS

$a_b$  = Set back distance between back of facing element and beam seat

$B$  = Base length of reinforcement not including the wall face

$b$  = Bearing width for bridge, beam seat

 $B_0$  = Width of the bridge
$$b_{\text{block}} = \text{Width of CMU}$$

$b_r$  = Length of bearing bed reinforcement

 $\theta_{RSF}$  = Width of RSF

$B_{\text{total}}$  = Total width at base of GRS abutment including the wall facing

CMU = Concrete masonry unit

$d_s$  = Clear space from top of wall to bottom of superstructure.

$d_{max}$  = Maximum particle diameter in reinforced backfill

$D_{RSF}$  = Depth of RSF below bottom of wall elevation

GRS = Geosynthetic Reinforced Soil

$H$  = Wall height measured from top of RSF to top of beam seat

$$H_{\text{CMU}} = \text{Height of CMU}$$

$h_{rb}$  = Height of road base (equals height of super structure and pavement thickness)

IBS = Integrated Bridge System

$L$  = Length of geosynthetic reinforcement

 $L_{abut}$  = Abutment width

$L_{block}$  = Length of CMU

$L_{\text{wet}}$  = Wingwall length

RSF = Reinforced soil /

$X_{\text{BSF}}$  = Length of BSF in front of  $t$

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WESTERN FEDERAL LANDS HIGHWAY DIVISION

## GRS-IBS

DESIGN DIMENSION  
QUANTITIES

NO.		DATE	BY	REVISIONS	NO.	DATE	BY	REVISIONS	DESIGNED BY	DRAWN BY	CHECKED BY	SCALE	PROJECT TEAM LEADER	BRIDGE DRAWING	DATE	DRAWING NO.
	03/25/11			Rev. 0					RHWA	C. TUTTLE	R. BARROWS, B. COLLINS, M. DOOSON, M. ELIAS A. ALZAMERA, J. NICKS	NTS	H. ADAMS	2 of 4	04/2011	









# CONSTRUCTION Youtube Video





















# User Perspective

## *Defiance County, Ohio*

Construction Costs:  
80'x32'-\$266,000 - 2005

Open to Traffic:  
47 days







**Construction Costs:**  
**28'x20'-\$68,000 - 2008**





Construction Costs  
28'x20'-\$88,000 - 20





**Construction Costs:**  
**32'x10'-\$51,000 - 2010**



201

Construction Costs:  
28'x20'-\$70,000 - 2010





Construction Costs:  
28'x20'-\$65,000 - 2010



201

Construction Costs:  
28'x32'-\$85,000 - 2010





200

Construction Costs:  
36'x20'-\$71,000 - 2010





Construction Cost:  
140'x40'-\$620,000 - 2009





# User Perspective

## *St. Lawrence County, NY*



CR 12 - 40'x33'- Material Cost \$160,000  
Construction costs \$240,000





**CR 24 - 47'x33'- Material Cost \$110,500**





CR 31 - 56'x33'- Material Cost \$165,000





CR 35 - 67'x33'- Material Cost \$180,500  
Construction Cost \$310,000





CR 38 - 63'x32' - Material Cost \$175,000





# User Perspective Huston Township, Pennsylvania







# User Perspective Ottawa County , Oklahoma

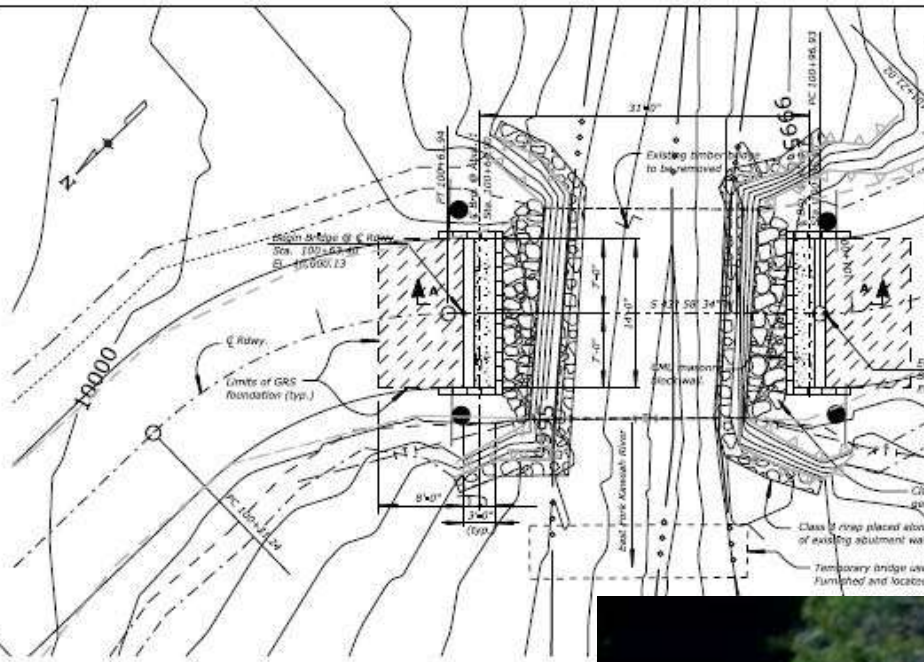






# User Perspective National Park Service

# Disney Bridge in Sequoia NP





# Strawberry Creek Great Basin National Park - NV





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Administration



# PROGRESS TOWARD 2012 EDC GRS IBD GOALS



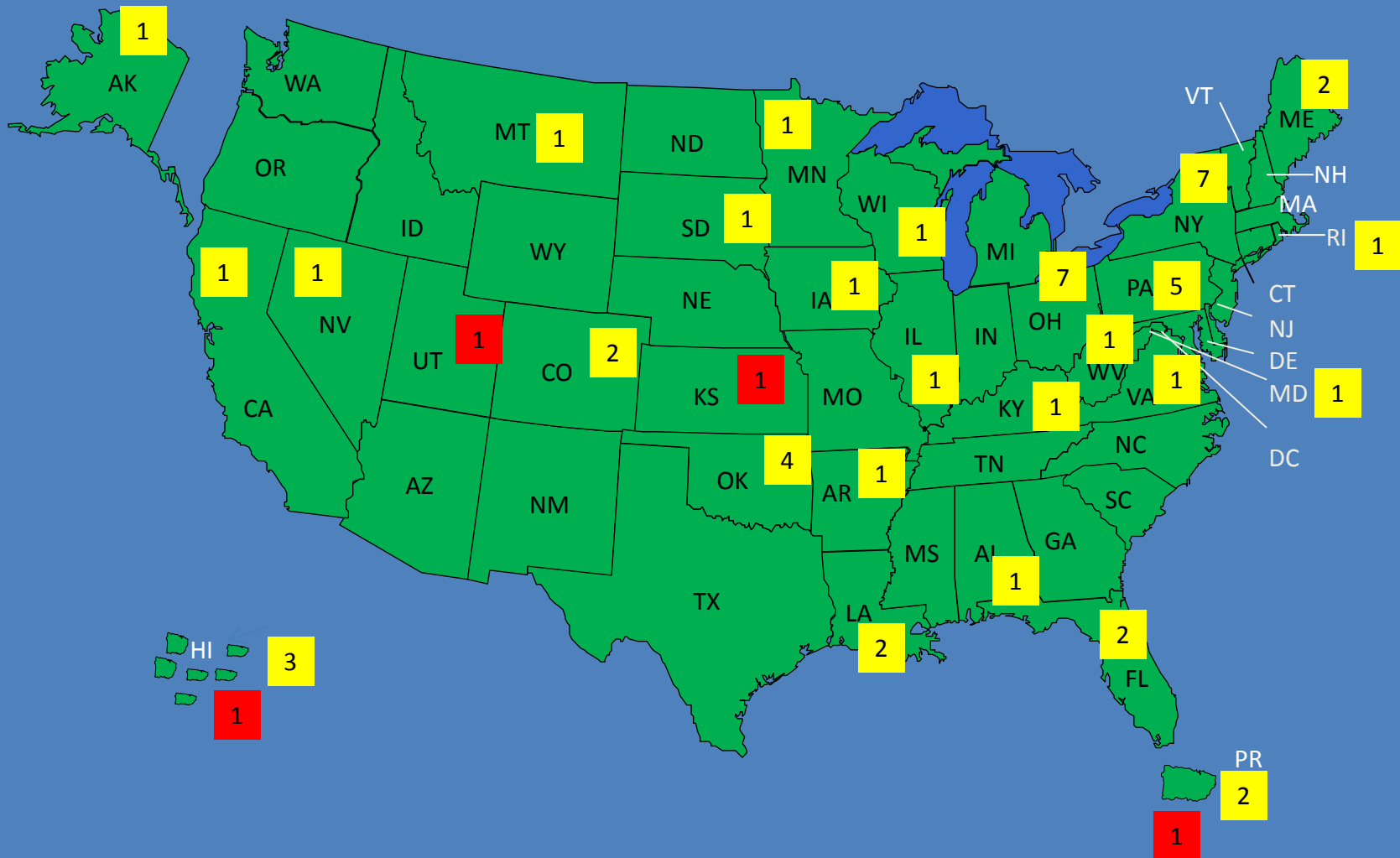


# 2012 Deployment Goals

- December 2012:
  - 30 bridges have been designed and/or constructed using GRS-IBS on the NHS within 20 states
  - 75 bridges have been designed and/or constructed using GRS-IBS off the NHS

# State DOT Deployment

Total of 56 project in 28 states at some stage of development from conceptual to construction







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